

INTERNATIONAL BEAMS

## LVL - Limit States Design Guide

The

## GREEN

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## Our Company

At International Beams, Inc. we take pride in providing our customers with premium quality products and services. Our LVL is manufactured to provide consistent, high performance floor and roof systems.

Our technical services consist of highly trained technical experts available to assist you with any design or construction question and to provide full support for our software.


## About LVL

Providing the superior performance and durability of engineered wood, International Beams, Inc. LVL is perfectly suited to spans bearing heavy loads and multi-span applications. The normal problems associated with increased lumber sizes - like decreased dimensional stability and uniformity - do not apply to our LVL, which utilizes ultrasonically tested and graded Douglas Fir veneer with evenly dispersed natural defects.

## Engineered for Quality

Checking is minimized because International Beams, Inc. LVL is cured in a controlled process in which waterproof adhesives boost stability and reduce warps and twists. All products are machineripped to generate uniform size and rigid, flat surfaces with inherently superior nail-holding characteristics.

We are confident that our products will provide our customers with consistent high performance when handled and installed in accordance with our Installation Guide.

Tested for strength and engineered for quality, International Beams, Inc. LVL represents our ongoing commitment to unsurpassed performance and service.


## General notes for this product guide:

1. All tables assume dry conditions. Calculations are based on CSA Standard 086-09 and the National Building Code of Canada (NBCC).
2. Lateral support of the compression edge of all beams must be provided at $24^{\prime \prime}$ on center.
3. Application tables include live load reductions applied in accordance with the NBCC.
4. Tables apply to Dead, Floor Live, Roof Live and Snow loads. Lateral loads must be considered by the building designer.
5. This design manual is intended to be used for preliminary design purposes; a complete structural analysis should be preformed by a design professional.
6. Beams that are $1^{3} 4^{\prime \prime} \times 16^{\prime \prime}$ and deeper require multiple plies.

### 2.0E LVL Design Properties

Factored Resistance (Standard Term) - 13/4"

| Depth <br> (in) | Factored Shear Resistance $V_{\text {r }}$ (lb) | Factored <br> Moment Resistance $\mathrm{M}_{\mathrm{r}}(\mathrm{lb})$ | $\begin{gathered} \mathrm{El} \\ \left(\mathrm{lb} . \mathrm{in}^{2} \times 10^{6}\right) \end{gathered}$ | Weight (plf) |
| :---: | :---: | :---: | :---: | :---: |
| 51/2 | 3113 | 4363 | 49 | 2.8 |
| 71/4 | 4103 | 7213 | 111 | 3.7 |
| 91/4 | 5235 | 11237 | 231 | 4.7 |
| 91/2 | 5377 | 11796 | 250 | 4.8 |
| $11^{1 / 4}$ | 6367 | 16046 | 415 | 5.7 |
| 117/8 | 6721 | 17706 | 488 | 6.1 |
| 14 | 7923 | 23891 | 800 | 7.1 |
| 16 | 9055 | 30463 | 1195 | 8.2 |
| 18 | 10187 | 37746 | 1701 | 9.2 |
| 20 | 11319 | 45725 | 2333 | 10.2 |
| 22 | 12451 | 54386 | 3106 | 11.2 |
| 24 | 13583 | 63718 | 4032 | 12.3 |

Factored Resistance (Standard Term) - 3½"

| Depth (in) | Factored Shear Resistance $\mathrm{V}_{\mathrm{r}}$ (lb) | Factored Moment Resistance $\mathrm{M}_{\mathrm{r}}$ (lb) | $\begin{gathered} \mathrm{EI} \\ \left(\mathrm{lb} . \mathrm{in}^{2} \times 10^{6}\right) \\ \hline \end{gathered}$ | Weight (plf) |
| :---: | :---: | :---: | :---: | :---: |
| 51/2 | 6225 | 8725 | 97 | 5.6 |
| $71 / 4$ | 8206 | 14425 | 222 | 7.4 |
| 91/4 | 10470 | 22474 | 462 | 9.4 |
| 91/2 | 10753 | 23592 | 500 | 9.7 |
| $11^{1 / 4}$ | 12734 | 32093 | 831 | 11.5 |
| 11\% $/ 8$ | 13441 | 35411 | 977 | 12.1 |
| 14 | 15847 | 47782 | 1601 | 14.3 |
| 16 | 18110 | 60927 | 2389 | 16.3 |
| 18 | 20374 | 75493 | 3402 | 18.4 |
| 20 | 22638 | 91450 | 4667 | 20.4 |
| 22 | 24902 | 108772 | 6211 | 22.5 |
| 24 | 27166 | 127437 | 8064 | 24.5 |

Notes:

1. The values have been calculated in accordance with CSA Standard 086-09.
2. The values are valid for dry service conditions, single member applications, standard term loading, and no treatment. Full lateral support is required for the compression edge, and both edges in the case of cantilevered and continuous beams.
3. Specified Strengths for $3100 \mathrm{Fb}-2.0 \mathrm{E}$ grade LVL for the beam orientation (edgewise):

Bending $\mathrm{f}_{\mathrm{b}}{ }^{*}=5729 \mathrm{psi}$
Shear $\mathrm{f}_{\mathrm{v}}=539 \mathrm{psi}$
Modulus of Elasticity $\mathrm{E}=2.0 \times 10^{6} \mathrm{psi}$
Compression perpendicular to grain $\mathrm{f}_{\mathrm{cp}}=1365 \mathrm{psi}$
Compression parallel to grain $f_{c}=5107$ psi
*Adjust $\mathrm{f}_{\mathrm{b}}$ by a factor of $(12 / \mathrm{d})^{0.18}$ where $\mathrm{d}=$ depth (in).

### 2.0E LVL Floor Beams



## Application Table - 2.0E Floor Beams - 13/4" Width

| Width of Building | Beam Span |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 11' | 12' | 13' | $14^{\prime}$ | 15' | 16' | $17^{\prime}$ | 18' | 19' | $20^{\prime}$ |
| 24' | 2-111/4 | 2-111/4 | 2-11\% ${ }^{1}$ | 2-14 | 2-14 | 2-16 | 2-16 | 2-16 | 2-18 | 2-18 |
|  | 3-91/4 | 3-91/2 | 3-111/4 | 3-111/4 | 3-117/8 | 3-14 | 3-14 | 3-14 | 3-16 | 3-16 |
| 28' | 2-111/4 | 2-111/4 | 2-14 | 2-14 | 2-14 | 2-16 | 2-16 | 2-18* | 2-18* | 3-16 |
|  | 3-91/4 | 3-111/4 | 3-111/4 | 3-117\%8 | 3-14 | 3-14 | 3-14 | 3-16 | 3-16 | 4-16 |
| 32' | 2-111/4 | 2-11/8 | 2-14 | 2-14 | 2-16 | 2-16* | 2-18* | 2-18* | 2-18* | 3-18 |
|  | 3-91/2 | 3-111/4 | 3-111/4 | 3-11\% ${ }^{\text {d }}$ | 3-14 | 3-14 | 3-16 | 3-16 | 3-16 | 4-16 |
| 36' | 2-111/4 | 2-14 | 2-14 | 2-14 | 2-16* | 2-16* | 2-18* | 2-18* | 3-16 | 3-18 |
|  | 3-111/4 | 3-111/4 | 3-117\% | 3-14 | 3-14 | 3-14 | 3-16 | 3-16 | 4-16 | 4-16 |
| $40^{\prime}$ | 2-11 ${ }^{\text {\% }}$ \% | 2-14 | 2-14* | 2-16* | 2-16* | 2-18* | 2-18* | 2-18* | 3-18 | 3-18 |
|  | 3-111/4 | 3-111/4 | 3-117/8 | 3-14 | 3-14 | 3-16 | 3-16 | 3-16 | 4-16 | 4-16 |

## Notes:

1. The table indicates the number of $13 / 4$ " wide LVL plies to be used for the given application.
2. Beam Span is the distance from centre to centre of supports, and is based on the more restrictive of simple or continuous span. The ratio of the short span to the long span should be greater than 0.4.
3. The beam must be centered in the building if the floor joists are continuous over the top. The beam may be located off-centre and the "width of building" may be taken as $80 \%$ of the actual width if the joists are simply supported and hang from the face of the beam.
4. Live load deflection is limited to $\mathrm{L} / 360$. Total load deflection, including beam weight, is limited to $\mathrm{L} / 240$.
5. The table is based on an unfactored live load of 40 psf, and an unfactored dead load of 12 psf .
6. Provide a minimum $3^{\prime \prime}$ bearing at each end, $7 \frac{1}{2}$ " bearing length at interior supports (* indicates that $41 / 2^{\prime \prime}$ is required at end supports and $11 \frac{1}{4}$ " at interior supports). Bearing length is based on the compression perpendicular resistance of the LVL. For bearing on materials with a lower compressive resistance the designer shall calculate the required bearing length.
7. Calculations are in accordance with CSA 086-09 and the National Building Code of Canada. Live loads have been reduced in accordance with 4.1.5.9 (3) of the NBCC. Vibration has not been considered.

These tables provide two selections for supporting roof loads over standard garage-door openings in various conditions.

| Width of Building | 25 psf snow load |  |  | 30 psf snow load |  |  | 40 psf snow load |  |  | 50 psf snow load |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  |
|  | 9'3" | 16'3" | 18' 3" | 9'3" | 16' 3" | 18'3" | 9'3" | 16' 3" | 18'3" | 9'3" | 16' 3" | $18^{\prime} 3^{\prime \prime}$ |
| $20^{\prime}$ | 2-71/4 | 2-14 | 2-14 | 2-91/4 | 2-14 | 2-16 | 2-91/4 | 2-14 | 2-16 | 2-91/4 | 2-16 | 2-18 |
|  | 3-71/4 | 3-111/4 | 3-14 | 3-71/4 | 3-111/4 | 3-14 | 3-71/4 | 3-14 | 3-14 | 3-91/4 | 3-14 | 3-16 |
| $24^{\prime}$ | 2-91/4 | 2-14 | 2-16 | 2-91/4 | 2-14 | 2-16 | 2-91/4 | 2-16 | 2-18 | 2-91/4 | 2-16* | 2-18* |
|  | 3-71/4 | $3-117 / 8$ | 3-14 | 3-71/4 | $3-117 / 8$ | 3-14 | 3-91/4 | 3-14 | 3-16 | 3-91/4 | 3-14 | 3-16 |
| 28' | 2-91/4 | 2-14 | 2-16 | 2-91/4 | 2-16 | 2-16 | 2-91/4 | 2-16 | 2-18* | 2-91/2 | 2-18* | 3-18 |
|  | 3-71/4 | $3-11{ }^{7} 8$ | 3-14 | 3-71/4 | 3-14 | 3-14 | 3-91/4 | 3-14 | 3-16 | $3-91 / 4$ | 3-16 | - |
| 32' | 2-91/4 | 2-16 | 2-16 | 2-91/4 | 2-16 | 2-18* | 2-91/4 | 2-18* | 3-16 | 2-111/4 | 2-18* | 3-18 |
|  | 3-71/4 | 3-14 | 3-14 | 3-91/4 | 3-14 | 3-16 | 3-91/4 | 3-14 | - | $3-91 / 4$ | 3-16 | - |
| 36' | 2-91/4 | 2-16 | 2-18* | 2-91/4 | 2-16* | 2-18* | 2-111/4 | 2-18* | 3-18 | 2-111/4 | 2-18* | 3-18* |
|  | 3-71/4 | 3-14 | 3-16 | 3-91/4 | 3-14 | 3-16 | 3-91/4 | 3-16 | - | 3-91/4 | 3-16 | - |



Notes:

1. The table indicates the number of $13 / 4$ " wide LVL plies to be used for the given application.
2. The listed span is the clear distance from face to face of supports. The design is based on a simple span for the unfactored roof loads shown in the table.
3. The roof structure is assumed to span from exterior wall to exterior wall and have a $24^{\prime \prime}$ overhang.
4. An unfactored live load of 10 psf has been included for an attic space with limited accessibility above the second floor ceiling.
5. Live load deflection is limited to $L / 360$. Total load deflection, including beam weight, is limited to $\mathrm{L} / 240$.
6. Provide a minimum $3^{\prime \prime}$ bearing at each end (* indicates that $4 \frac{1}{2}$ " is required). Bearing length is based on the compression perpendicular resistance of the LVL.

For bearing on materials with a lower compressive resistance the designer shall calculate the required bearing length.
7. Calculations are in accordance with CSA 086-09 and the National Building Code of Canada. Live loads have been reduced in accordance with 4.1.5.9 (3) of the NBCC. Vibration and creep have not been considered.

Accounting for a second-story floor and wall, these tables provide two selections for supporting roof loads over standard garage-door openings in various conditions.

## 2-Storey Application Table - 2.0E Garage Door Headers - $13 / 4$ " Width

| Width of Building | 25 psf snow load |  |  | 30 psf snow load |  |  | 40 psf snow load |  |  | 50 psf snow load |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  |
|  | 9'3" | $16^{\prime \prime}{ }^{\prime \prime}$ | 18'3" | 9'3" | 16'3" | 18'3" | 9'3" | 16' ${ }^{\prime \prime}$ | 18'3" | 9'3" | 16' ${ }^{\prime \prime}$ | 18'3" |
| $20^{\prime}$ | 2-91/4 | 2-14 | 2-16 | 2-91/4 | 2-16 | 2-18 | 2-91/4 | 2-16 | 2-18* | 2-91/4 | 2-16* | 2-18* |
|  | 3-71/4 | 3-14 | 3-14 | 3-71/4 | 3-14 | 3-14 | 3-91/4 | 3-14 | 3-16 | 3-91/4 | 3-14 | 3-16 |
| 24' | 2-91/4 | 2-16 | 2-18 | 2-91/4 | 2-16 | 2-18* | 2-91/4 | 2-16* | 2-18* | 2-91/2 | 2-18* | 3-18 |
|  | 3-71/4 | 3-14 | 3-16 | 3-91/4 | 3-14 | 3-16 | 3-91/4 | 3-14 | 3-16 | 3-91/4 | 3-16 |  |
| 28' | 2-91/4 | 2-16 | 2-18* | 2-91/4 | 2-16* | 2-18* | 2-91/2 | 2-18* | 3-18 | 2-111/4 | 2-18* | 3-18* |
|  | $3-91 / 4$ | 3-14 | 3-16 | 3-91/4 | 3-14 | 3-16 | 3-91/4 | 3-16 |  | $3-91 / 4$ | 3-16 |  |
| 32' | 2-91/4 | 2-16* | 2-18* | 2-91/2 | 2-18* | 3-16 | 2-111/4 | 2-18* | 3-18* | 2-111/4 | 3-16* | 3-18* |
|  | 3-71/4 | 3-14 | 3-16 | 3-91/4 | 3-16 |  | 3-91/4 | 3-16 |  | 3-91/4 | - | - |
| 36' | 2-91/2 | 2-18* | 3-18 | 2-111/4 | 2-18* | 3-18 | 2-111/4 | 3-16* | 3-18* | 2-111/4* | 3-18* | - |
|  | 3-91/4 | 3-16 | - | 3-91/4 | 3-16 | - | 3-91/4 | - | - | $3-91 / 2$ | - | - |



Notes:

1. The table indicates the number of $13 / 4^{4}$ wide LVL plies to be used for the given application.
2. The listed span is the clear distance from face to face of supports. The design is based on a simple span for the unfactored roof loads shown in the table.
3. The roof structure is assumed to span from exterior wall to exterior wall and have a 24 " overhang.
4. The floor joists must be supported at the centre of the building by a wall or beam.
5. The table is based on an unfactored floor live load of 40 psf, and an unfactored floor dead load of 12 psf. An unfactored dead load of 80 plf has been included for the second floor wall, and an unfactored live load of 10 psf has been included for an attic space with limited accessibility above the second floor ceiling.
6. Live load deflection is limited to $\mathrm{L} / 360$. Total load deflection, including beam weight, is limited to $\mathrm{L} / 240$.
7. Provide a minimum 3" bearing at each end (* indicates that $41 / 2^{\prime \prime}$ is required). Bearing length is based on the compression perpendicular resistance of the LVL. For bearing on materials with a lower compressive resistance the designer shall calculate the required bearing length.
8. Calculations are in accordance with CSA 086-09 and the National Building Code of Canada. Live loads have been reduced in accordance with 4.1.5.9 (3) of the NBCC. Vibration and creep have not been considered.

### 2.0E LVL Window \& Door Headers

These tables provide two selections for supporting roof loads over rough openings in various conditions.


| 1-Storey Application Table - 2.0E Window \& Door Headers - 13/4" Width |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\left\|\begin{array}{c} \text { Width } \\ \text { of } \\ \text { Building } \end{array}\right\|$ | 25 psf snow load |  |  |  |  | 30 psf snow load |  |  |  |  | 40 psf snow load |  |  |  |  | 50 psf snow load |  |  |  |  |
|  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  |
|  | $6^{1}$ | $8{ }^{\prime}$ | $9{ }^{\prime}$ | 10' | 12' | $6^{\prime}$ | $8^{\prime}$ | 9' | 10' | 12' | $6^{1}$ | $8^{\prime}$ | $9^{\prime}$ | 10' | 12' | $6{ }^{\prime}$ | $8{ }^{\prime}$ | $9^{\prime}$ | 10' | 12' |
| $20^{\prime}$ | 2-51/2 | 2-71/4 | 2-71/4 | 2-91/4 | 2-91/4 | 2-51/2 | 2-71/4 | 2-71/4 | 2-91/4 | 2-91/4 | 2-51/2 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-71/4 | 2-91/4 | 2-91/4 | 2-91/4 | 2-111/4 |
|  | $3-51 / 2$ | 3-51/2 | 3-71/4 | 3-71/4 | 3-91/4 | 3-51/2 | 3-51/2 | 3-71/4 | 3-71/4 | 3-91/4 | 3-51/2 | 3-71/4 | 3-71/4 | 3-91/4 | 3-91/4 | 3-51/2 | 3-71/4 | 3-71/4 | 3-91/4 | 3-111/4 |
| 24' | 2-51/2 | 2-71/4 | 2-71/4 | 2-91/4 | 2-11/4 | 2-51/2 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-51/2 | 2-91/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-71/4 | 2-91/4 | 291/4 | 2-111/4 | 2-117/8 |
|  | 3-51/2 | 3-71/4 | 3-71/4 | 3-71/4 | 3-91/4 | 3-51/2 | 3-71/4 | 3-71/4 | 3-71/4 | 3-91/4 | 3-51/2 | 3-71/4 | 3-71/4 | 3-91/4 | 3-91/2 | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 |
| 28' | 2-51/2 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-51/2 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-71/4 | 2-91/4 | 2-91/4 | 2-11/4 | 2-117/8 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-14 |
|  | 3-51/2 | 3-71/4 | 3-71/4 | 3-71/4 | 3-91/4 | 3-51/2 | 3-71/4 | 3-71/4 | 3-91/4 | 3-91/4 | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 |
| 32' | 2-51/2 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-51/2 | 2-91/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-71/4 | 2-91/4 | 2-91/4 | 2-11/4 | 2-14 | 2-71/4 | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 |
|  | $3-51 / 2$ | 3-71/4 | 3-71/4 | 3-91/4 | 3-91/4 | 3-51/2 | 3-71/4 | 3-71/4 | 3-91/4 | 3-91/2 | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-71/4 | 3-91/4 | 3-91/4 | 3-91/4 | 3-111/4 |
| 36' | 2-51/2 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-71/4 | 2-91/4 | 2-91/4 | 2-91/2 | 2-111/8 | 2-71/4 | 2-91/4 | 2-91/2 | 2-111/4 | 2-14 | 2-71/4 | 2-91/4 | 2-111/4 | 2-111/4 | 2-14* |
|  | 3-51/2 | 3-71/4 | 3-71/4 | 3-91/4 | 3-91/2 | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-71/4 | 3-91/4 | $3-91 / 4$ | 3-111/4 | 3-11/8 |

Notes:

1. The table indicates the number of $1^{3 / 4} 4^{\text {" }}$ wide LVL plies to be used for the given application.
2. The listed span is the clear distance from face to face of supports. The design is based on a simple span for the unfactored roof loads shown in the table.
3. The roof structure is assumed to span from exterior wall to exterior wall and have a 24 " overhang.
4. An unfactored live load of 10 psf has been included for an attic space with limited accessibility above the second floor ceiling.
5. Live load deflection is limited to L/360. Total load deflection, including beam weight, is limited to L/240.
6. Provide a minimum 3" bearing at each end (* indicates that $4^{1} / 2^{\prime \prime}$ is required). Bearing length is based on the compression perpendicular resistance of the LVL. For bearing on materials with a lower compressive resistance the designer shall calculate the required bearing length.
7. Calculations are in accordance with CSA 086-09 and the National Building Code of Canada. Live loads have been reduced in accordance with 4.1.5.9 (3) of the NBCC. Vibration and creep have not been considered.

Accounting for a second-story floor and wall, these tables provide two selections for supporting roof loads over rough openings in various conditions.


2-Storey Application Table - 2.0E Window \& Door Headers - $13 / 4$ " Width

| Width of Building | 25 psf snow load |  |  |  |  | 30 psf snow load |  |  |  |  | 40 psf snow load |  |  |  |  | 50 psf snow load |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  |
|  | $6^{\prime}$ | 8' | 9' | $10^{\prime}$ | 12' | $6^{\prime}$ | 8' | 9' | 10' | 12' | $6^{\prime}$ | 8' | 9' | 10' | 12' | $6^{\prime}$ | 8' | 9' | 10' | 12' |
| $20^{\prime}$ | 2-51/2 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-51/2 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-5 $1 / 2$ | 2-91/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-1178 |
|  | 3-51/2 | $3-71 / 4$ | $3-71 / 4$ | 3-91/4 | $3-91 / 4$ | 3-51/2 | $3-71 / 4$ | 3-71/4 | $3-91 / 4$ | $3-91 / 4$ | $3-51 / 2$ | 3-71/4 | $3-711_{4}$ | $3-91 / 4$ | $3-11 \frac{1}{4}$ | $3-51 / 2$ | $3-71 / 4$ | $3-91 / 4$ | 3-91/4 | 3-111/4 |
| 24' | 2-51/2 | $2-71 / 4$ | 2-91/4 | $2-91 / 4$ | 2-111/4 | 2-71/4 | 2-91/4 | 2-91/4 | 2-91/4 | 2-111/4 | $2-7 \frac{1}{2}$ | 2-91/4 | 2-91/4 | 2-111/4 | 2-117\% | $2-7 \frac{1}{4}$ | 2-91/4 | $2-91 / 4$ | 2-111/4 | 2-14 |
|  | 3-51/2 | 3-71/4 | 3-71/4 | 3-91/4 | 3-91/2 | 3-51/2 | 3-71/4 | $3-71 / 4$ | $3-91 / 4$ | 3-111/4 | $3-51 / 2$ | $3-71 / 4$ | $3-91 / 4$ | $3-91 / 4$ | 3-111/4 | $3-51 / 2$ | $3-71 / 4$ | $3-911_{4}$ | 3-91/4 | 3-111/4 |
| 28' | 2-71/4 | 2-91/4 | 2-91/4 | 2-91/2 | 2-117/8 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-117/8 | $2-7 \frac{1 / 4}{}$ | 2-91/4 | 2-91/4 | 2-111/4 | 2-14 | $2-71 / 4$ | 2-91/4 | 2-111/4 | 2-111/4 | 2-14* |
|  | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-51/2 | $3-71 / 4$ | $3-91 / 4$ | 3-91/4 | 3-111/4 | $3-51 / 2$ | $3-71 / 4$ | $3-91 / 4$ | $3-91 / 4$ | 3-111/4 | $3-71 / 2$ | 3-91/4 | $3-911_{4}$ | 3-91/2 | 3-111/4 |
| 32' | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | $2-11^{1 / 8}$ | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-14 | 2-71/4 | 2-91/4 | 2-111/4 | 2-111/4 | 2-14* | $2-71 / 4$ | 2-91/4 | 2-111/4 | 2-111/4 | 2-14* |
|  | 3-51/2 | $3-71 / 4$ | 3-91/4 | $3-91 / 4$ | 3-111/4 | 3-51/2 | $3-7 \frac{1}{4}$ | $3-91 / 4$ | $3-91 / 4$ | 3-111/4 | $3-7 \frac{1}{2}$ | 3-91/4 | $3-91 / 4$ | $3-91 / 4$ | 3-111/4 | $3-71 / 4$ | 3-91/4 | $3-9114$ | 3-111/4 | 3-1178 |
| 36' | 2-71/4 | $2-91 / 4$ | 2-91/4 | 2-111/4 | 2-14 | 2-71/4 | 2-91/4 | 2-91/2 | 2-111/4 | 2-14 | $2-7 \frac{1}{4}$ | 2-91/4 | 2-111/4 | 2-111/4 | 2-14* | $2-71 / 4$ | 2-91/2 | 2-111/4 | 2-117/8** | 2-16* |
|  | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | $3-7 \frac{1}{2}$ | 3-91/4 | 3-91/4 | 3-111/4 | 3-117\% | $3-71 / 4$ | 3-91/4 | 3-91/4 | 3-111/4 | 3-14 |

Notes:

1. The table indicates the number of $13 / 4$ " wide LVL plies to be used for the given application.
2. The listed span is the clear distance from face to face of supports. The design is based on a simple span for the unfactored roof loads shown in the table.
3. The roof structure is assumed to span from exterior wall to exterior wall and have a 24 " overhang.
4. The floor joists must be supported at the centre of the building by a wall or beam.
5. The table is based on an unfactored floor live load of 40 psf, and an unfactored floor dead load of 12 psf . An unfactored dead load of 80 plf has been included for the second floor wall, and an unfactored live load of 10 psf has been included for an attic space with limited accessibility above the second floor ceiling.
6. Live load deflection is limited to $\mathrm{L} / 360$. Total load deflection, including beam weight, is limited to L/240.
7. Provide a minimum $3^{\prime \prime}$ bearing at each end (* indicates that $4^{1} / 2^{2}$ is required). Bearing length is based on the compression perpendicular resistance of the LVL. For bearing on materials with a lower compressive resistance the designer shall calculate the required bearing length.
8. Calculations are in accordance with CSA 086-09 and the National Building Code of Canada. Live loads have been reduced in accordance with 4.1.5.9 (3) of the NBCC. Vibration and creep have not been considered.

# 2.0E LVL Uniform Load <br> Resistance (plf) - Floor 100\% 13/4" 

## Uniform Load Resistance (plf) - 2.0E- Floor 100\%-13/4" Width

| Span (ft) | $1^{3 / 4^{11}} \times 7{ }^{1 / 4^{\prime \prime}}$ |  |  |  | $13^{3 / 4}{ }^{11} \times 91 /{ }^{1 /}$ |  |  |  | $1^{3 / 4^{11}} \times 9^{1 / 2^{\prime \prime}}$ |  |  |  | $1^{3 / 4^{\prime \prime}} \times 11^{1 / 4^{\prime \prime}}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistanc | Unfactored Defl. Resistance |  |  | $\square$ |
|  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \\ & \hline \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \end{aligned}$ |  |
|  | L/480 | L/360 |  |  | L/480 | L/360 |  |  | L/480 | L/360 |  |  | L/480 | L/360 |  |  |
| 6 | 571 | 762 | 1139 | 1299 | 1187 | 1583 |  | 1751 | 1286 | 1715 |  | 1811 | 2136 |  |  | 2256 |
| 7 | 360 | 480 | 716 | 1083 | 747 | 997 |  | 1446 | 810 | 1080 |  | 1494 | 1345 | 1793 |  | 1845 |
| 8 | 241 | 321 | 478 | 896 | 500 | 667 | 997 | 1231 | 542 | 723 | 1080 | 1271 | 901 | 1201 |  | 1560 |
| 9 | 169 | 225 | 335 | 707 | 351 | 469 | 698 | 1072 | 381 | 508 | 757 | 1106 | 632 | 843 | 1260 | 1351 |
| 10 | 123 | 164 | 243 | 572 | 256 | 341 | 508 | 893 | 277 | 370 | 550 | 937 | 461 | 615 | 917 | 1191 |
| 11 | 92 | 123 | 181 | 472 | 192 | 256 | 380 | 737 | 208 | 278 | 412 | 773 | 346 | 462 | 687 | 1053 |
| 12 | 71 | 95 | 139 | 396 | 148 | 197 | 292 | 618 | 160 | 214 | 316 | 649 | 267 | 356 | 528 | 884 |
| 13 | 56 | 74 | 108 | 336 | 116 | 155 | 228 | 526 | 126 | 168 | 248 | 552 | 210 | 280 | 414 | 752 |
| 14 | 45 | 60 | 86 | 289 | 93 | 124 | 182 | 452 | 101 | 135 | 197 | 475 | 168 | 224 | 330 | 647 |
| 15 | - | 48 | 69 | 251 | 75 | 101 | 147 | 393 | 82 | 109 | 159 | 413 | 136 | 182 | 267 | 563 |
| 16 | - | 40 | 56 | 220 | 62 | 83 | 120 | 345 | 67 | 90 | 130 | 362 | 112 | 150 | 219 | 494 |
| 17 | - | - | - | - | 52 | 69 | 99 | 305 | 56 | 75 | 108 | 320 | 93 | 125 | 182 | 437 |
| 18 | - | - | - | - | 43 | 58 | 83 | 271 | 47 | 63 | 90 | 285 | 79 | 105 | 152 | 389 |
| 20 | - | - | - | - | - | 42 | 59 | 218 | - | 46 | 64 | 229 | 57 | 76 | 109 | 313 |
| 22 | - | - | - | - | - | - | - | - | - | - | - | - | 43 | 57 | 80 | 258 |
| 24 | - | - | - | - | - | - | - | - | - | - | - | - | - | 44 | 61 | 215 |
| 26 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 28 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 30 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 32 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 34 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Span (ft) | $1^{3 / 4}{ }^{11} \times 11^{7 / 8}{ }^{\text {" }}$ |  |  |  | $1^{3 / 4}{ }^{11} \times 14^{\prime \prime}$ |  |  |  | $1^{3 / 4} 4^{\prime \prime} \times 16^{\prime \prime}$ |  |  |  | $1^{3 / 4}{ }^{\text {" }} \times 18^{\text {" }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | $\begin{gathered} \text { Factored } \\ \text { Total } \\ \text { Resistance } \end{gathered}$ | Unfactored Defl. Resistance |  |  | $\square$ |
|  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \\ & \hline \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \end{aligned}$ |  |
|  | L/480 | L/360 |  |  | L/480 | L/360 |  |  | L/480 | L/360 |  |  | L/480 | L/360 |  |  |
| 6 | - | - | - | 2427 | - | - | - | 3058 | - | - | - | 3736 | - | - | - | 4516 |
| 7 | 1582 | - | - | 1977 | - | - | - | 2460 | - | - | - | 2967 | - | - | - | 3532 |
| 8 | 1059 | 1413 | - | 1668 | 1736 | - | - | 2058 | - | - | - | 2459 | - | - | - | 2899 |
| 9 | 744 | 992 | - | 1442 | 1219 | 1626 | - | 1768 | 1820 | - | - | 2099 | - | - | - | 2458 |
| 10 | 542 | 723 | 1079 | 1270 | 889 | 1185 | - | 1549 | 1327 | 1769 | - | 1831 | 1890 | - | - | 2133 |
| 11 | 407 | 543 | 809 | 1134 | 668 | 890 | 1329 | 1379 | 997 | 1329 | - | 1624 | 1419 | - | - | 1884 |
| 12 | 314 | 418 | 622 | 976 | 514 | 686 | 1022 | 1242 | 768 | 1024 | - | 1458 | 1093 | 1458 | - | 1686 |
| 13 | 247 | 329 | 488 | 830 | 404 | 539 | 802 | 1122 | 604 | 805 | 1200 | 1323 | 860 | 1147 | - | 1526 |
| 14 | 197 | 263 | 389 | 715 | 324 | 432 | 641 | 966 | 483 | 644 | 959 | 1210 | 688 | 918 | 1368 | 1393 |
| 15 | 160 | 214 | 315 | 622 | 263 | 351 | 519 | 840 | 393 | 524 | 778 | 1073 | 560 | 746 | 1110 | 1282 |
| 16 | 132 | 176 | 259 | 545 | 217 | 289 | 427 | 737 | 324 | 432 | 640 | 941 | 461 | 615 | 913 | 1168 |
| 17 | 110 | 147 | 214 | 482 | 181 | 241 | 354 | 652 | 270 | 360 | 532 | 833 | 384 | 512 | 760 | 1033 |
| 18 | 93 | 124 | 180 | 429 | 152 | 203 | 297 | 581 | 227 | 303 | 447 | 742 | 324 | 432 | 639 | 920 |
| 20 | 67 | 90 | 129 | 346 | 111 | 148 | 215 | 469 | 165 | 221 | 323 | 599 | 236 | 315 | 463 | 743 |
| 22 | 50 | 67 | 95 | 285 | 83 | 111 | 160 | 386 | 124 | 166 | 241 | 493 | 177 | 236 | 345 | 612 |
| 24 | - | 52 | 72 | 238 | 64 | 85 | 121 | 323 | 96 | 128 | 184 | 413 | 136 | 182 | 264 | 512 |
| 26 | - | 41 | 55 | 202 | 50 | 67 | 94 | 273 | 75 | 100 | 143 | 350 | 107 | 143 | 206 | 435 |
| 28 | - | - | - | - | 40 | 54 | 74 | 235 | 60 | 80 | 112 | 300 | 86 | 114 | 163 | 373 |
| 30 | - | - | - | - | - | 43 | 58 | 203 | 49 | 65 | 90 | 260 | 70 | 93 | 130 | 324 |
| 32 | - | - | - | - | - | - | - | - | 40 | 54 | 73 | 227 | 57 | 76 | 106 | 283 |
| 34 | - | - | - | - | - | - | - | - | - | 45 | 59 | 200 | 48 | 64 | 87 | 249 |

## Notes:

1. The values in these tables meet the requirements of the National Building Code of Canada and CSA Standard 086-09 for dry service conditions and standard term loads. The live load must be greater than the dead load in order to use these tables.
2. All values listed are based on uniform loads applied to the top of the beam.
3. Span is defined as centre-to-centre of bearings and is valid for simple span and equal, continuous span conditions.
4. These tables assume full lateral support of the compression edge.
5. The designer must check both the Factored Total Resistance and the Total L/240 Deflection Resistance, AND the appropriate Live Load column, either the L/480 or L/360 deflection limit. Unfactored Deflection Resistance values that are blank are governed by the Factored Total Resistance.
6. The Unfactored Deflection Resistance for Total L/240 does not include the effects of long term loading (creep).
7. The total load values have been adjusted to account for the self-weight of the beam.
8. Proper bearing must be provided at each support. The required bearing can be determined from the Maximum Factored Reaction Table.
9. Depths of $16^{\prime \prime}$ or greater should be used with a minimum of two plies.
10. The values in this table are for a single ply of $13 / 4$ " LVL. Double the values for a 2 -ply ( $31 / 2^{\prime \prime}$ thick) beam, triple the values for a 3 -ply ( $51 / 4$ " thick) beam, and quadruple the values for 4-ply (7" thick) beam.

### 2.0E LVL Uniform Load <br> Resistance (plf) - Floor 100\% 13/4"

Uniform Load Resistance (plf) - 2.0E- Floor 100\%-13/4" Width

| Span <br> (ft) | $13^{\prime \prime}{ }^{\prime \prime} \times 20^{\prime \prime}$ |  |  |  | $13 / 4^{\prime \prime} \times 22^{\prime \prime}$ |  |  |  | $1^{3 / 4}{ }^{\text {" }}$ x $24^{\prime \prime}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance |
|  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | Live Load |  | Total L/240 |  | Live Load |  | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  |
|  | L/480 | L/360 |  |  | L/480 | L/360 |  |  | L/480 | L/360 |  |  |
| 6 | - | - | - | 5420 | - | - | - | 6482 | - | - | - | 7746 |
| 7 | - | - | - | 4166 | - | - | - | 4884 | - | - | - | 5704 |
| 8 | - | - | - | 3383 | - | - | - | 3918 | - | - | - | 4512 |
| 9 | - | - | - | 2847 | - | - | - | 3269 | - | - | - | 3731 |
| 10 | - | - | - | 2457 | - | - | - | 2805 | - | - | - | 3180 |
| 11 | 1947 | - | - | 2160 | - | - | - | 2455 | - | - | - | 2771 |
| 12 | 1500 | - | - | 1927 | 1996 | - | - | 2183 | - | - | - | 2454 |
| 13 | 1180 | 1573 | - | 1740 | 1570 | - | - | 1965 | 2039 | - | - | 2202 |
| 14 | 944 | 1259 | - | 1585 | 1257 | 1676 | - | 1786 | 1632 | - | - | 1997 |
| 15 | 768 | 1024 | - | 1455 | 1022 | 1363 | - | 1637 | 1327 | 1769 | - | 1826 |
| 16 | 632 | 843 | 1255 | 1345 | 842 | 1123 | - | 1510 | 1093 | 1458 | - | 1682 |
| 17 | 527 | 703 | 1045 | 1251 | 702 | 936 | 1393 | 1402 | 911 | 1215 | - | 1559 |
| 18 | 444 | 592 | 879 | 1116 | 591 | 788 | 1172 | 1308 | 768 | 1024 | - | 1453 |
| 20 | 324 | 432 | 638 | 901 | 431 | 575 | 851 | 1073 | 560 | 746 | 1107 | 1259 |
| 22 | 243 | 324 | 476 | 743 | 324 | 432 | 637 | 885 | 420 | 560 | 829 | 1038 |
| 24 | 187 | 250 | 365 | 622 | 249 | 332 | 488 | 741 | 324 | 432 | 636 | 869 |
| 26 | 147 | 196 | 285 | 528 | 196 | 261 | 381 | 629 | 254 | 339 | 497 | 739 |
| 28 | 118 | 157 | 226 | 454 | 157 | 209 | 303 | 541 | 204 | 272 | 396 | 635 |
| 30 | 96 | 128 | 182 | 393 | 127 | 170 | 244 | 469 | 165 | 221 | 319 | 551 |
| 32 | 79 | 105 | 148 | 344 | 105 | 140 | 199 | 411 | 136 | 182 | 261 | 482 |
| 34 | 65 | 87 | 121 | 303 | 87 | 117 | 164 | 362 | 113 | 151 | 215 | 425 |

Notes:

1. The values in these tables meet the requirements of the National Building Code of Canada and CSA Standard 086-09 for dry service conditions and standard term loads. The live load must be greater than the dead load in order to use these tables.
2. All values listed are based on uniform loads applied to the top of the beam.
3. Span is defined as centre-to-centre of bearings and is valid for simple span and equal, continuous span conditions.
4. These tables assume full lateral support of the compression edge.
5. The designer must check both the Factored Total Resistance and the Total L/240 Deflection Resistance, AND the appropriate Live Load column, either the L/480 or L/360 deflection limit. Unfactored Deflection Resistance values that are blank are governed by the Factored Total Resistance.
6. The Unfactored Deflection Resistance for Total L/240 does not include the effects of long term loading (creep).
7. The total load values have been adjusted to account for the self-weight of the beam.
8. Proper bearing must be provided at each support. The required bearing can be determined from the Maximum Factored Reaction Table.
9. Depths of $16^{\prime \prime}$ or greater should be used with a minimum of two plies.
10. The values in this table are for a single ply of $1^{3 / 1} 4^{\text {" }}$ LVL. Double the values for a 2 -ply ( $3^{1} / 2^{\prime \prime}$ thick) beam, triple the values for a 3 -ply ( $5^{1} / 4^{\prime \prime}$ thick) beam, and quadruple the values for 4-ply (7" thick) beam.

### 2.0E LVL Uniform Load <br> Resistance (plf) - Roof $100 \% 1^{3} 4^{\prime \prime}$

## Uniform Load Resistance (plf) - 2.0E- Roof $100 \%-13 / 4$ " Width

| Span (ft) | $1^{3 / 4^{\prime \prime}} \times 71 / 4^{\prime \prime}$ |  |  |  | $1^{3 / 4}{ }^{17} \times 9^{1 / 4}{ }^{17}$ |  |  |  | $1^{3 / 4^{11}} \times{ }^{1 / 1 / 2^{\prime \prime}}$ |  |  |  | $1^{3 / 4^{\prime \prime}} \times 11^{1 / 4^{\prime \prime}}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | $\square$$\begin{array}{\|c\|} \text { Factored } \\ \text { Total } \\ \text { Resistance } \\ \hline \end{array}$ | Unfactored Defl. Resistance |  |  | Factored Total Resistance |
|  | Live Load |  | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | Total <br> L/180 |  | Live Load |  | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  |
|  | L/360 | L/240 |  |  | L/360 | L/240 |  |  | L/360 | L/240 |  |  | L/360 | L/240 |  |  |
| 6 | 762 | 1143 | - | 1299 | 1583 | - | - | 1751 | 1715 | - | - | 1811 | - | - | - | 2256 |
| 7 | 480 | 720 | 956 | 1083 | 997 | - | - | 1446 | 1080 | - | - | 1494 | 1793 | - | - | 1845 |
| 8 | 321 | 482 | 639 | 896 | 667 | 1001 | - | 1231 | 723 | 1085 | - | 1271 | 1201 | - | - | 1560 |
| 9 | 225 | 338 | 448 | 707 | 469 | 703 | 933 | 1072 | 508 | 762 | 1011 | 1106 | 843 | 1265 |  | 1351 |
| 10 | 164 | 246 | 325 | 572 | 341 | 512 | 679 | 893 | 370 | 555 | 736 | 937 | 615 | 922 |  | 1191 |
| 11 | 123 | 185 | 243 | 472 | 256 | 385 | 509 | 737 | 278 | 417 | 551 | 773 | 462 | 693 | 918 | 1053 |
| 12 | 95 | 142 | 186 | 396 | 197 | 296 | 391 | 618 | 214 | 321 | 423 | 649 | 356 | 534 | 706 | 884 |
| 13 | 74 | 112 | 146 | 336 | 155 | 233 | 306 | 526 | 168 | 252 | 332 | 552 | 280 | 420 | 554 | 752 |
| 14 | 60 | 90 | 116 | 289 | 124 | 186 | 244 | 452 | 135 | 202 | 265 | 475 | 224 | 336 | 442 | 647 |
| 15 | 48 | 73 | 93 | 251 | 101 | 151 | 197 | 393 | 109 | 164 | 214 | 413 | 182 | 273 | 358 | 563 |
| 16 | 40 | 60 | 76 | 220 | 83 | 125 | 162 | 345 | 90 | 135 | 176 | 362 | 150 | 225 | 294 | 494 |
| 17 | - | 50 | 63 | 195 | 69 | 104 | 134 | 305 | 75 | 113 | 145 | 320 | 125 | 187 | 244 | 437 |
| 18 | - | 42 | 52 | 173 | 58 | 87 | 112 | 271 | 63 | 95 | 122 | 285 | 105 | 158 | 205 | 389 |
| 20 | - | - | - | - | 42 | 64 | 80 | 218 | 46 | 69 | 87 | 229 | 76 | 115 | 148 | 313 |
| 22 | - | - | - | - | - | 48 | 59 | 179 | - | 52 | 64 | 188 | 57 | 86 | 109 | 258 |
| 24 | - | - | - | - | - | - | - | - | - | 40 | 48 | 157 | 44 | 66 | 83 | 215 |
| 26 | - | - | - | - | - | - | - | - | - | - | - | - | - | 52 | 64 | 182 |
| 28 | - | - | - | - | - | - | - | - | - | - | - | - | - | 42 | 50 | 156 |
| 30 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 32 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 34 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Span (ft) | $1^{3 / 4}{ }^{11} \times 11^{7 / 8^{\prime \prime}}$ |  |  |  | $1^{3 / 4} 4^{17} \times 14^{\prime \prime}$ |  |  |  | $1^{3 / 4}{ }^{11} \times 16^{11}$ |  |  |  | $1^{3 / 4} 4^{17} \times 18^{\prime \prime}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | FactoredTotalResistance | Unfactored Defl. Resistance |  |  | Factored <br> Total <br> Resistance |
|  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  |
|  | L/360 | L/240 |  |  | L/360 | L/240 |  |  | L/360 | L/240 |  |  | L/360 | L/240 |  |  |
| 6 | - | - | - | 2427 | - | - | - | 3058 | - | - | - | 3736 | - | - | - | 4516 |
| 7 | - | - | - | 1977 | - | - | - | 2460 | - | - | - | 2967 | - | - | - | 3532 |
| 8 | 1413 | - | - | 1668 | - | - | - | 2058 | - | - | - | 2459 | - | - | - | 2899 |
| 9 | 992 | - | - | 1442 | 1626 | - | - | 1768 | - | - | - | 2099 | - | - | - | 2458 |
| 10 | 723 | 1085 | - | 1270 | 1185 | - | - | 1549 | 1769 | - | - | 1831 | - | - | - | 2133 |
| 11 | 543 | 815 | 1081 | 1134 | 890 | 1336 | - | 1379 | 1329 | - | - | 1624 | - | - | - | 1884 |
| 12 | 418 | 628 | 831 | 976 | 686 | 1029 | - | 1242 | 1024 | - | - | 1458 | 1458 | - | - | 1686 |
| 13 | 329 | 494 | 652 | 830 | 539 | 809 | 1072 | 1122 | 805 | 1208 | - | 1323 | 1147 | - | - | 1526 |
| 14 | 263 | 395 | 521 | 715 | 432 | 648 | 857 | 966 | 644 | 967 | - | 1210 | 918 | 1377 | - | 1393 |
| 15 | 214 | 321 | 422 | 622 | 351 | 526 | 695 | 840 | 524 | 786 | 1040 | 1073 | 746 | 1120 | - | 1282 |
| 16 | 176 | 264 | 347 | 545 | 289 | 434 | 571 | 737 | 432 | 648 | 856 | 941 | 615 | 922 | - | 1168 |
| 17 | 147 | 220 | 288 | 482 | 241 | 362 | 475 | 652 | 360 | 540 | 712 | 833 | 512 | 769 | 1016 | 1033 |
| 18 | 124 | 186 | 242 | 429 | 203 | 304 | 399 | 581 | 303 | 455 | 598 | 742 | 432 | 648 | 855 | 920 |
| 20 | 90 | 135 | 174 | 346 | 148 | 222 | 289 | 469 | 221 | 331 | 434 | 599 | 315 | 472 | 620 | 743 |
| 22 | 67 | 101 | 129 | 285 | 111 | 167 | 215 | 386 | 166 | 249 | 324 | 493 | 236 | 354 | 464 | 612 |
| 24 | 52 | 78 | 98 | 238 | 85 | 128 | 164 | 323 | 128 | 192 | 248 | 413 | 182 | 273 | 355 | 512 |
| 26 | 41 | 61 | 76 | 202 | 67 | 101 | 127 | 273 | 100 | 151 | 193 | 350 | 143 | 215 | 277 | 435 |
| 28 | - | 49 | 59 | 173 | 54 | 81 | 101 | 235 | 80 | 120 | 153 | 300 | 114 | 172 | 220 | 373 |
| 30 | - | 40 | 47 | 149 | 43 | 65 | 80 | 203 | 65 | 98 | 123 | 260 | 93 | 140 | 177 | 324 |
| 32 | - | - | - | - | - | 54 | 65 | 177 | 54 | 81 | 100 | 227 | 76 | 115 | 144 | 283 |
| 34 | - | - | - | - | - | 45 | 53 | 156 | 45 | 67 | 82 | 200 | 64 | 96 | 119 | 249 |

## Notes:

1. The values in these tables meet the requirements of the National Building Code of Canada and CSA Standard 086-09 for dry service conditions and standard term loads. The live load must be greater than the dead load in order to use these tables.
2. All values listed are based on uniform loads applied to the top of the beam.
3. Span is defined as centre-to-centre of bearings and is valid for simple span and equal, continuous span conditions.
4. These tables assume full lateral support of the compression edge.
5. The designer must check both the Factored Total Resistance and the Total L/180 Deflection Resistance, AND the appropriate Live Load column, either the L/360 or L/240 deflection limit. Unfactored Deflection Resistance values that are blank are governed by the Factored Total Resistance.
6. The Unfactored Deflection Resistance for Total L/180 does not include the effects of long term loading (creep).
7. The total load values have been adjusted to account for the self-weight of the beam.
8. Proper bearing must be provided at each support. The required bearing can be determined from the Maximum Factored Reaction Table.
9. Depths of $16^{\prime \prime}$ or greater should be used with a minimum of two plies.
10. The values in this table are for a single ply of $1 \frac{3}{4}$ " LVL. Double the values for a 2 -ply ( $3^{1 / 2}{ }^{\prime \prime}$ thick) beam, triple the values for a 3 -ply ( $51 / 4$ "thick) beam, and quadruple the values for 4-ply (7" thick) beam.

### 2.0E LVL Uniform Load <br> Resistance (plf) - Roof $\mathbf{1 0 0 \%}$ 13/4"

## Uniform Load Resistance (pifi) - 2.0E- Roof $100 \%-13 / 4$ " Width

| Span <br> (ft) | $13 / 4^{\prime \prime} \times 20^{\prime \prime}$ |  |  |  | $13 / 4^{\prime \prime} \times 22^{\prime \prime}$ |  |  |  | $13 / 4^{\prime \prime} \times 24^{\prime \prime}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance |
|  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | Total L/180 |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  |
|  | L/360 | L/240 |  |  | L/360 | L/240 |  |  | L/360 | L/240 |  |  |
| 6 | - | - | - | 5420 | - | - | - | 6482 | - | - | - | 7746 |
| 7 | - | - | - | 4166 | - | - | - | 4884 | - | - | - | 5704 |
| 8 | - | - | - | 3383 | - | - | - | 3918 | - | - | - | 4512 |
| 9 | - | - | - | 2847 | - | - | - | 3269 | - | - | - | 3731 |
| 10 | - | - | - | 2457 | - | - | - | 2805 | - | - | - | 3180 |
| 11 | - | - | - | 2160 | - | - | - | 2455 | - | - | - | 2771 |
| 12 | - | - | - | 1927 | - | - | - | 2183 | - | - | - | 2454 |
| 13 | 1573 | - | - | 1740 | - | - | - | 1965 | - | - | - | 2202 |
| 14 | 1259 | - | - | 1585 | 1676 | - | - | 1786 | - | - | - | 1997 |
| 15 | 1024 | - | - | 1455 | 1363 | - | - | 1637 | 1769 | - | - | 1826 |
| 16 | 843 | 1265 | - | 1345 | 1123 | - | - | 1510 | 1458 | - | - | 1682 |
| 17 | 703 | 1055 | - | 1251 | 936 | - | - | 1402 | 1215 | - | - | 1559 |
| 18 | 592 | 889 | - | 1116 | 788 | 1183 | - | 1308 | 1024 | - | - | 1453 |
| 20 | 432 | 648 | 854 | 901 | 575 | 862 | - | 1073 | 746 | 1120 | - | 1259 |
| 22 | 324 | 486 | 639 | 743 | 432 | 648 | 853 | 885 | 560 | 841 | - | 1038 |
| 24 | 250 | 375 | 490 | 622 | 332 | 499 | 654 | 741 | 432 | 648 | 852 | 869 |
| 26 | 196 | 295 | 383 | 528 | 261 | 392 | 512 | 629 | 339 | 509 | 667 | 739 |
| 28 | 157 | 236 | 304 | 454 | 209 | 314 | 408 | 541 | 272 | 408 | 532 | 635 |
| 30 | 128 | 192 | 246 | 393 | 170 | 255 | 329 | 469 | 221 | 331 | 430 | 551 |
| 32 | 105 | 158 | 200 | 344 | 140 | 210 | 269 | 411 | 182 | 273 | 352 | 482 |
| 34 | 87 | 131 | 165 | 303 | 117 | 175 | 223 | 362 | 151 | 227 | 291 | 425 |

Notes:

1. The values in these tables meet the requirements of the National Building Code of Canada and CSA Standard 086-09 for dry service conditions and standard term loads. The live load must be greater than the dead load in order to use these tables.
2. All values listed are based on uniform loads applied to the top of the beam.
3. Span is defined as centre-to-centre of bearings and is valid for simple span and equal, continuous span conditions.
4. These tables assume full lateral support of the compression edge.
5. The designer must check both the Factored Total Resistance and the Total L/180 Deflection Resistance, AND the appropriate Live Load column, either the L/360 or L/240 deflection limit. Unfactored Deflection Resistance values that are blank are governed by the Factored Total Resistance.
6. The Unfactored Deflection Resistance for Total L/180 does not include the effects of long term loading (creep).
7. The total load values have been adjusted to account for the self-weight of the beam.
8. Proper bearing must be provided at each support. The required bearing can be determined from the Maximum Factored Reaction Table.
9. Depths of $16^{\prime \prime}$ or greater should be used with a minimum of two plies.
10. The values in this table are for a single ply of $1 \frac{3}{4}$ " LVL. Double the values for a 2 -ply ( $3^{1} / 2^{\prime \prime}$ thick) beam, triple the values for a 3 -ply ( $5^{1 / 2}{ }^{\text {" }}$ thick) beam, and quadruple the values for 4-ply (7" thick) beam.

Factored Resistance (Standard Term) - 13/4"

| Depth (in) | Factored Shear Resistance $\mathrm{V}_{\mathrm{t}}$ (lb) | Factored Moment Resistance $\mathrm{M}_{\mathrm{r}}$ (lb) | $\begin{gathered} E I \\ \left(\mathrm{lb} . \mathrm{in}^{2} \times 10^{6}\right) \\ \hline \end{gathered}$ | Weight (plf) |
| :---: | :---: | :---: | :---: | :---: |
| 51/2 | 3061 | 3166 | 36 | 2.8 |
| 71/4 | 4035 | 5235 | 83 | 3.7 |
| $91 / 4$ | 5148 | 8156 | 173 | 4.7 |
| 91/2 | 5287 | 8561 | 188 | 4.8 |
| $11^{1 / 4}$ | 6261 | 11646 | 311 | 5.7 |
| 11\% $/ 8$ | 6608 | 12850 | 366 | 6.1 |
| 14 | 7791 | 17340 | 600 | 7.1 |
| 16 | 8904 | 22110 | 896 | 8.2 |
| 18 | 10017 | 27396 | 1276 | 9.2 |
| 20 | 11130 | 33186 | 1750 | 10.2 |
| 22 | 12243 | 39472 | 2329 | 11.2 |
| 24 | 13356 | 46246 | 3024 | 12.3 |

Factored Resistance (Standard Term) - 3½"

| Depth (in) | Factored Shear Resistance $\mathrm{V}_{\mathrm{r}}$ (lb) | Factored Moment Resistance $M_{\mathrm{r}}$ (lb) | $\begin{gathered} \mathrm{EI} \\ \left(\mathrm{lb} . \mathrm{in}^{2} \times 10^{6}\right) \\ \hline \end{gathered}$ | Weight (plf) |
| :---: | :---: | :---: | :---: | :---: |
| 51/2 | 6122 | 6333 | 73 | 5.6 |
| $71 / 4$ | 8069 | 10470 | 167 | 7.4 |
| $91 / 4$ | 10295 | 16311 | 346 | 9.4 |
| 91/2 | 10574 | 17123 | 375 | 9.7 |
| $11 \frac{1}{4}$ | 12521 | 23292 | 623 | 11.5 |
| 117/8 | 13217 | 25701 | 733 | 12.1 |
| 14 | 15582 | 34679 | 1201 | 14.3 |
| 16 | 17808 | 44219 | 1792 | 16.3 |
| 18 | 20034 | 54791 | 2552 | 18.4 |
| 20 | 22260 | 66373 | 3500 | 20.4 |
| 22 | 24486 | 78945 | 4659 | 22.5 |
| 24 | 26712 | 92491 | 6048 | 24.5 |

Notes:

1. The values have been calculated in accordance with CSA Standard 086-09.
2. The values are valid for dry service conditions, single member applications, standard term loading, and no treatment.

Full lateral support is required for the compression edge, and both edges in the case of cantilevered and continuous beams.
3. Specified Strengths for 2250Fb-1.5E grade LVL for the beam orientation (edgewise):

Bending $\mathrm{f}_{\mathrm{b}}{ }^{*}=4158 \mathrm{psi}$
Shear $\mathrm{f}_{\mathrm{v}}=530 \mathrm{psi}$
Modulus of Elasticity E $=1.5 \times 10^{6} \mathrm{psi}$
Compression perpendicular to grain $\mathrm{f}_{\mathrm{cp}}=1365 \mathrm{psi}$
Compression parallel to grain $f_{c}=3751$ psi
*Adjust $f_{b}$ by a factor of $(12 / \mathrm{d})^{0.18}$ where $d=$ depth (in).

### 1.5E LVL Floor Beams



## Application Table - 1.5E Floor Beams - $13 / 4$ " Width

| Width of Building | Beam Span |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 11' | 12' | $13^{\prime}$ | $14^{\prime}$ | 15' | 16' | $17{ }^{\prime}$ | 18' | 19' | $20^{\prime}$ |
| 24' | 2-111/4 | 2-117\% | 2-14 | 2-14 | 2-16 | 2-16 | 2-18 | 2-18 | 3-18 | 3-18 |
|  | 3-91/2 | 3-111/4 | 3-111/4 | 3-14 | 3-14 | 3-14 | 3-16 | 3-16 | 4-16 | 4-16 |
| 28' | 2-11 ${ }^{1} / 8$ | 2-14 | 2-14 | 2-16 | 2-16 | 2-18 | 2-18 | 3-16 | 3-18 | 3-18 |
|  | 3-111/4 | 3-111/4 | 3-117/8 | 3-14 | 3-14 | 3-16 | 3-16 | 4-16 | 4-16 | 4-16 |
| 32' | 2-117\% | 2-14 | 2-14 | 2-16 | 2-16 | 2-18* | 2-18* | 3-18 | 3-18 | 3-18 |
|  | 3-111/4 | 3-111/4 | 3-14 | 3-14 | 3-14 | 3-16 | 3-16 | 4-16 | 4-16 | 4-18 |
| $36^{\prime}$ | 2-14 | 2-14 | 2-16 | 2-16 | 2-18* | 2-18* | 3-16 | 3-18 | 3-18 | 4-18 |
|  | 3-111/4 | 3-117\% | 3-14 | 3-14 | 3-16 | 3-16 | 4-16 | 4-16 | 4-16 | - |
| $40^{\prime}$ | 2-14 | 2-14 | 2-16* | 2-16* | 2-18* | 2-18* | 3-18 | 3-18 | 4-18 | 4-18 |
|  | 3-111/4 | 3-14 | 3-14 | 3-14 | 3-16 | 3-16 | 4-16 | 4-16 | - | - |

## Notes:

1. The table indicates the number of $1 \frac{3}{4}$ " wide LVL plies to be used for the given application.
2. Beam Span is the distance from centre to centre of supports, and is based on the more restrictive of simple or continuous span. The ratio of the short span to the long span should be greater than 0.4.
3. The beam must be centered in the building if the floor joists are continuous over the top. The beam may be located off-centre and the "width of building" may be taken as $80 \%$ of the actual width if the joists are simply supported and hang from the face of the beam.
4. Live load deflection is limited to L/360. Total load deflection, including beam weight, is limited to L/240.
5. The table is based on an unfactored live load of 40 psf, and an unfactored dead load of 12 psf .
6. Provide a minimum $3^{\prime \prime}$ bearing at each end, $7 \frac{1}{2}$ " bearing length at interior supports (* indicates that $41 / 2^{\prime \prime}$ is required at end supports and $11 \frac{1}{4}$ " at interior supports). Bearing length is based on the compression perpendicular resistance of the LVL. For bearing on materials with a lower compressive resistance the designer shall calculate the required bearing length.
7. Calculations are in accordance with CSA 086-09 and the National Building Code of Canada. Live loads have been reduced in accordance with 4.1.5.9 (3) of the NBCC. Vibration has not been considered.

### 1.5E LVL Garage Door Headers

These tables provide two selections for supporting roof loads over standard garage-door openings in various conditions.

| dth | 25 psf snow load |  |  | 30 psf snow load |  |  | 40 psf snow load |  |  | 50 psf snow load |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  |
| Building | 9'3" | 16' 3" | 18'3" | 9'3" | 16'3" | 18'3" | 9'3" | 16' 3" | 18'3" | 9'3" | 16' 3" | 18'3" |
| 20' | 2-91/4 | 2-14 | 2-16 | 2-91/4 | 2-16 | 2-16 | 2-91/4 | 2-16 | 2-18 | 2-91/2 | 2-18 | 3-18 |
|  | 3-71/4 | $3-117 \%$ | 3-14 | 3-71/4 | 3-14 | 3-14 | 3-91/4 | 3-14 | 3-16 | $3-91 / 4$ | 3-16 | - |
| $24^{\prime}$ | 2-91/4 | 2-16 | 2-16 | $2-91 / 4$ | 2-16 | 2-18 | 2-91/4 | 2-18 | 3-16 | 2-111/4 | 2-18* | 3-18 |
|  | 3-71/4 | 3-14 | 3-14 | $3-91 / 4$ | 3-14 | 3-16 | 3-91/4 | 3-16 | - | $3-91 / 4$ | 3-16 | - |
| 28' | 2-91/4 | 2-16 | 2-18 | 2-91/4 | 2-16 | 2-18 | 2-111/4 | 2-18 | 3-18 | 2-111/4 | 3-16 | 3-18 |
|  | 3-91/4 | 3-14 | 3-16 | $3-91 / 4$ | 3-14 | 3-16 | $3-91 / 4$ | 3-16 | - | $3-91 / 4$ | - | - |
| 32' | 2-91/4 | 2-16 | 2-18 | 2-91/4 | 2-18 | 3-16 | 2-111/4 | 2-18* | 3-18 | 2-111/4 | 3-18 | - |
|  | 3-91/4 | 3-14 | 3-16 | $3-91 / 4$ | 3-16 | - | $3-91 / 4$ | 3-16 | - | 3-91/2 | - | - |
| 36' | 2-91/4 | 2-18 | 3-16 | 2-111/4 | 2-18* | 3-18 | 2-111/4 | 3-16 | 3-18 | 2-111/4 | 3-18 | - |
|  | 3-91/4 | 3-14 | - | 3-91/4 | 3-16 | - | 3-91/4 | - | - | 3-111/4 | - | - |



Notes:

1. The table indicates the number of $1^{3} / 4^{4}$ wide LVL plies to be used for the given application.
2. The listed span is the clear distance from face to face of supports. The design is based on a simple span for the unfactored roof loads shown in the table.
3. The roof structure is assumed to span from exterior wall to exterior wall and have a 24 " overhang.
4. An unfactored live load of 10 psf has been included for an attic space with limited accessibility above the second floor ceiling.
5. Live load deflection is limited to $\mathrm{L} / 360$. Total load deflection, including beam weight, is limited to $\mathrm{L} / 240$.
6. Provide a minimum 3" bearing at each end (* indicates that $4 \frac{1}{2}{ }^{\prime \prime}$ is required). Bearing length is based on the compression perpendicular resistance of the LVL. For bearing on materials with a lower compressive resistance the designer shall calculate the required bearing length.
7. Calculations are in accordance with CSA 086-09 and the National Building Code of Canada. Live loads have been reduced in accordance with 4.1.5.9 (3) of the NBCC. Vibration and creep have not been considered.

Accounting for a second-story floor and wall, these tables provide two selections for supporting roof loads over standard garage-door openings in various conditions.

| WidthofBuilding | 25 psf snow load |  |  | 30 psf snow load |  |  | 40 psf snow load |  |  | 50 psf snow load |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  | 15 psf roof dead load |  |  |
|  | 9'3" | 16' 3" | 18' ${ }^{\prime \prime}$ | 9' 3" | $16^{\prime \prime} 3^{\prime \prime}$ | 18'3" | 9'3" | 16' 3" | 18' 3" | 9' 3" | 16' 3" | 18'3" |
| $20^{\prime}$ | 2-91/4 | 2-16 | 2-18 | 2-91/4 | 2-16 | 2-18 | 2-91/2 | 2-18 | 3-18 | 2-111/4 | 2-18* | 3-18 |
|  | 3-91/4 | 3-14 | 3-16 | 3-91/4 | 3-14 | 3-16 | 3-91/4 | 3-16 | - | $3-91 / 4$ | 3-16 | - |
| $24^{\prime}$ | 2-91/4 | 2-18 | 3-16 | 2-91/2 | 2-18 | 3-18 | 2-111/4 | 2-18* | 3-18 | 2-111/4 | 3-16 | 3-18 |
|  | 3-91/4 | 3-16 | - | $3-91 / 4$ | 3-16 | - | $3-91 / 4$ | 3-16 | - | 3-91/4 | - | - |
| $28^{\prime}$ | 2-111/4 | 2-18 | 3-18 | 2-111/4 | 2-18* | 3-18 | 2-111/4 | 3-16 | 3-18 | 2-111/4 | 3-18 | - |
|  | $3-91 / 4$ | 3-16 | - | 3-91/4 | 3-16 | - | $3-91 / 4$ | - | - | $3-11 \frac{1}{4}$ | - | - |
| $32^{\prime}$ | 2-111/4 | 2-18* | 3-18 | 2-111/4 | 3-16 | 3-18 | 2-111/4 | 3-18 | - | 2-11 ${ }^{\text {\% }}$ | 3-18* | - |
|  | $3-91 / 4$ | 3-16 | - | 3-91/4 | - | - | 3-91/2 | - | - | $3-11 \frac{1}{4}$ | - | - |
| 36 | 2-111/4 | 3-16 | 3-18 | 2-111/4 | 3-18 | - | 2-117/8 | 3-18* | - | 2-14* | - | - |
|  | $3-91 / 4$ | - | - | 3-91/4 | - | - | 3-111/4 | - | - | 3-111/4 | - | - |



Notes:

1. The table indicates the number of $13 / 4^{\prime \prime}$ wide LVL plies to be used for the given application.
2. The listed span is the clear distance from face to face of supports. The design is based on a simple span for the unfactored roof loads shown in the table.
3. The roof structure is assumed to span from exterior wall to exterior wall and have a 24 " overhang.
4. The floor joists must be supported at the centre of the building by a wall or beam.
5. The table is based on an unfactored floor live load of 40 psf, and an unfactored floor dead load of 12 psf. An unfactored dead load of 80 plf has been included for the second floor wall, and an unfactored live load of 10 psf has been included for an attic space with limited accessibility above the second floor ceiling."
6. Live load deflection is limited to L/360. Total load deflection, including beam weight, is limited to L/240.
7. Provide a minimum 3" bearing at each end (* indicates that $41 / 2 "$ is required). Bearing length is based on the compression perpendicular resistance of the LVL. For bearing on materials with a lower compressive resistance the designer shall calculate the required bearing length.
8. Calculations are in accordance with CSA 086-09 and the National Building Code of Canada. Live loads have been reduced in accordance with 4.1.5.9 (3) of the NBCC. Vibration and creep have not been considered.

### 1.5E LVL Window <br> \& Door Headers

These tables provide two selections for supporting roof loads over rough openings in various conditions.


1-Storey Application Table - 1.5E Window \& Door Headers - $13 / 4$ " Width

| Width of Building | 25 psf snow load |  |  |  |  | 30 psf snow load |  |  |  |  | 40 psf snow load |  |  |  |  | 50 psf snow load |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  |
|  | $6^{\prime}$ | 8' | 9' | 10' | 12' | $6^{\prime}$ | 8' | 9' | 10' | 12' | $6^{\prime}$ | 8' | 9' | 10' | 12' | $6^{1}$ | 8' | 9' | 10' | 12' |
| $20^{\prime}$ | 2-51/2 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-51/2 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-71/4 | 2-91/4 | 2-91/4 | 2-91/2 | 2-117\% | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-14 |
|  | 3-51/2 | 3-71/4 | 3-71/4 | $3-7 \frac{1}{4}$ | $3-91 / 4$ | 3-51/2 | 3-71/4 | 3-71/4 | 3-91/4 | $3-91 / 4$ | 3-51/2 | 3-71/4 | 3-91/4 | $3-91 / 4$ | 3-111/4 | $3-51 / 2$ | 3-71/4 | 3-91/4 | $3-91 / 4$ | 3-111/4 |
| 24' | 2-51/2 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-51/2 | 2-91/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-14 | $2-7 \frac{1}{4}$ | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 |
|  | 3-51/2 | 3-71/4 | 3-71/4 | $3-91 / 4$ | 3-91/4 | 3-51/2 | $3-71 / 4$ | 3-71/4 | 3-91/4 | 3-111/4 | $3-51 / 2$ | $3-71 / 4$ | 3-91/4 | 3-91/4 | 3-111/4 | $3-71 / 4$ | 3-91/4 | 3-91/4 | $3-91 / 2$ | 3-111/4 |
| 28' | 2-51/2 | 2-91/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-117\% | 2-71/4 | 2-91/4 | 2-91/2 | 2-111/4 | 2-14 | $2-71 / 4$ | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 |
|  | 3-51/2 | $3-71 / 4$ | $3-71 / 4$ | $3-91 / 4$ | 3-111/4 | $3-51 / 2$ | 3-71/4 | 3-91/4 | $3-911_{4}$ | 3-111/4 | $3-51 / 2$ | $3-91 / 4$ | 3-91/4 | $3-91 / 4$ | 3-111/4 | $3-71 / 4$ | 3-91/4 | $3-91 / 4$ | 3-111/4 | 3-117/8 |
| 32' | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-117/8 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-14 | $2-71 / 4$ | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 | $2-71 / 4$ | 2-91/2 | 2-111/4 | 2-117\% | 2-16 |
|  | 3-51/2 | 3-71/4 | $3-91 / 4$ | $3-91 / 4$ | 3-111/4 | $3-51 / 2$ | $3-71 / 4$ | 3-91/4 | $3-91 / 4$ | 3-111/4 | $3-71 / 4$ | 3-91/4 | 3-91/4 | $3-91 / 2$ | 3-117\% | $3-71 / 4$ | $3-91 / 4$ | $3-91 / 4$ | 3-111/4 | 3-14 |
| 36' | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-117/8 | 2-71/4 | 2-91/4 | 2-91/2 | 2-111/4 | 2-14 | $2-711_{4}$ | 2-91/4 | 2-111/4 | 2-117\% | 2-14 | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 | 2-16* |
|  | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-117\% | $3-71 / 4$ | 3-91/4 | 3-91/2 | 3-111/4 | 3-14 |

Notes:

1. The table indicates the number of $13 / 4$ " wide LVL plies to be used for the given application.
2. The listed span is the clear distance from face to face of supports. The design is based on a simple span for the unfactored roof loads shown in the table.
3. The roof structure is assumed to span from exterior wall to exterior wall and have a 24 " overhang.
4. An unfactored live load of 10 psf has been included for an attic space with limited accessibility above the second floor ceiling.
5. Live load deflection is limited to $\mathrm{L} / 360$. Total load deflection, including beam weight, is limited to $\mathrm{L} / 240$.
6. Provide a minimum 3" bearing at each end (* indicates that $41 / 2^{\prime \prime}$ is required). Bearing length is based on the compression perpendicular resistance of the LVL. For bearing on materials with a lower compressive resistance the designer shall calculate the required bearing length.
7. Calculations are in accordance with CSA 086-09 and the National Building Code of Canada. Live loads have been reduced in accordance with 4.1.5.9 (3) of the NBCC. Vibration and creep have not been considered.

Accounting for a second-story floor and wall, these tables provide two selections for supporting roof loads over rough openings in various conditions.


2-Storey Application Table - 1.5E Window \& Door Headers - $13 / 4$ " Width

| WidthofBuilding | 25 psf snow load |  |  |  |  | 30 psf snow load |  |  |  |  | 40 psf snow load |  |  |  |  | 50 psf snow load |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  | 15 psf roof dead load |  |  |  |  |
|  | $6^{\prime}$ | 8' | 9' | $10^{\prime}$ | 12' | $6^{\prime}$ | $8^{\prime}$ | 9' | 10' | 12' | $6^{\prime}$ | 8' | 9' | 10' | 12' | $6^{\prime}$ | 8' | 9' | 10' | 12' |
| 20' | 2-71/4 | 2-91/4 | 2-91/4 | 2-91/2 | 2-117\% | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | $2-117_{8}$ | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-14 | 2-71/4 | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 |
|  | 3-51/2 | $3-71 / 4$ | 3-91/4 | 3-91/4 | 3-111/4 | 3-51/2 | 3-71/4 | $3-91 / 4$ | 3-91/4 | 3-111/4 | $3-51 / 2$ | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-71/4 | 3-91/4 | 3-91/4 | $3-91 / 2$ | 3-111/4 |
| 24' | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-14 | 2-71/4 | 2-91/4 | 2-91/4 | 2-111/4 | 2-14 | 2-71/4 | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 | 2-71/4 | 2-91/4 | 2-111/4 | 2-117\% | 2-14 |
|  | 3-51/2 | $3-71 / 4$ | 3-91/4 | $3-91 / 4$ | 3-111/4 | 3-51/2 | $3-71 / 4$ | $3-91 / 4$ | $3-91 / 4$ | 3-111/4 | $3-71 / 4$ | 3-91/4 | $3-91 / 4$ | $3-91 / 4$ | 3-111/4 | 3-71/4 | 3-91/4 | 3-91/4 | $3-11 \frac{1}{4}$ | 3-1178 |
| 28' | 2-71/4 | 2-91/4 | 2-91/2 | 2-111/4 | 2-14 | 2-71/4 | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 | 2-71/4 | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 | 2-71/4 | 2-91/2 | 2-111/4 | 2-117\% | 2-16* |
|  | 3-51/2 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-71/4 | 3-91/4 | $3-91 / 4$ | 3-91/4 | 3-111/4 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-117\% | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-14 |
| $32^{\prime}$ | 2-71/4 | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 | 2-71/4 | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 | 2-71/4 | 2-91/2 | 2-111/4 | 2-117\% | 2-16* | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 | 2-16* |
|  | 3-71/4 | $3-91 / 4$ | 3-91/4 | $3-91 / 2$ | 3-117/8 | 3-71/4 | 3-91/4 | $3-91 / 4$ | 3-111/4 | 3-117/8 | 3-71/4 | 3-91/4 | 3-91/4 | 3-111/4 | 3-14 | 3-71/4 | 3-91/4 | 3-111/4 | 3-111/4 | 3-14 |
| 36' | 2-71/4 | $2-91 / 4$ | 2-111/4 | 2-111/4 | 2-14 | 2-71/4 | 2-91/4 | 2-111/4 | 2-117/8 | 2-14 | 2-91/4 | 2-111/4 | 2-111/4 | 2-14 | 2-16* | 2-91/4 | 2-111/4 | $2-11 \%_{8}$ | 2-14* | 2-18* |
|  | 3-71/4 | $3-91 / 4$ | 3-91/4 | 3-111/4 | 3-117\% | 3-71/4 | 3-91/4 | $3-91 / 4$ | 3-111/4 | 3-14 | 3-71/4 | $3-91 / 4$ | 3-91/2 | 3-111/4 | 3-14 | 3-71/4 | 3-91/4 | 3-111/4 | 3-111/4 | 3-14 |

## Notes:

1. The table indicates the number of $13 / 4$ " wide LVL plies to be used for the given application.
2. The listed span is the clear distance from face to face of supports. The design is based on a simple span for the unfactored roof loads shown in the table.
3. The roof structure is assumed to span from exterior wall to exterior wall and have a 24 " overhang.
4. The floor joists must be supported at the centre of the building by a wall or beam.
5. The table is based on an unfactored floor live load of 40 psf , and an unfactored floor dead load of 12 psf . An unfactored dead load of 80 plf has been included for the second floor wall, and an unfactored live load of 10 psf has been included for an attic space with limited accessibility above the second floor ceiling.
6. Live load deflection is limited to $\mathrm{L} / 360$. Total load deflection, including beam weight, is limited to $\mathrm{L} / 240$.
7. Provide a minimum $3^{\prime \prime}$ bearing at each end (* indicates that $41 / 2^{\prime \prime}$ is required). Bearing length is based on the compression perpendicular resistance of the LVL. For bearing on materials with a lower compressive resistance the designer shall calculate the required bearing length.
8. Calculations are in accordance with CSA 086-09 and the National Building Code of Canada. Live loads have been reduced in accordance with 4.1.5.9 (3) of the NBCC. Vibration and creep have not been considered.

### 1.5E LVL Uniform Load

Resistance (plf) - Floor 100\% 13/4"

## Uniform Load Resistance (plf) - 1.5E- Floor 100\%-13/4" Width

| Span (ft) | $1^{3 / 4}{ }^{11} \times 7{ }^{1 / 4}{ }^{\text {" }}$ |  |  |  | $13^{3 / 4}{ }^{11} \times 91 /{ }^{1 /}$ |  |  |  | $1^{3 / 4^{11}} \times 9^{1 / 2^{\prime \prime}}$ |  |  |  | $1^{3 / 4^{\prime \prime}} \times 11^{1 / 4^{\prime \prime}}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  |  | Unfactored Defl. Resistance |  |  | FactoredTotalResistance | Unfactored Defl. Resistance |  |  | $\square$$\begin{array}{\|c\|} \text { Factored } \\ \text { Total } \\ \text { Resistance } \\ \hline \end{array}$ | Unfactored Defl. Resistance |  |  | Factored <br> Total <br> Resistance |
|  | Live Load |  | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | Live Load |  | Total |  | Live Load |  | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \end{aligned}$ |  |
|  | L/480 | L/360 |  |  | L/480 | L/360 |  |  | L/480 | L/360 |  |  | L/480 | L/360 |  |  |
| 6 | 428 | 571 | 853 | 1158 | 890 | 1187 | - | 1722 | 964 | 1286 | - | 1781 | 1602 | 2136 | - | 2218 |
| 7 | 270 | 360 | 536 | 850 | 560 | 747 | 1116 | 1325 | 607 | 810 | 1210 | 1391 | 1008 | 1345 |  | 1814 |
| 8 | 180 | 241 | 358 | 649 | 375 | 500 | 746 | 1013 | 407 | 542 | 809 | 1064 | 675 | 901 | 1346 | 1448 |
| 9 | 127 | 169 | 250 | 512 | 263 | 351 | 523 | 799 | 285 | 381 | 566 | 839 | 474 | 632 | 943 | 1143 |
| 10 | 92 | 123 | 181 | 414 | 192 | 256 | 380 | 646 | 208 | 277 | 411 | 678 | 346 | 461 | 686 | 924 |
| 11 | 69 | 92 | 135 | 341 | 144 | 192 | 284 | 533 | 156 | 208 | 308 | 560 | 260 | 346 | 514 | 762 |
| 12 | 53 | 71 | 103 | 286 | 111 | 148 | 217 | 447 | 120 | 160 | 236 | 469 | 200 | 267 | 394 | 639 |
| 13 | 42 | 56 | 80 | 243 | 87 | 116 | 170 | 380 | 94 | 126 | 184 | 399 | 157 | 210 | 309 | 544 |
| 14 | - | 45 | 63 | 209 | 70 | 93 | 135 | 327 | 75 | 101 | 147 | 343 | 126 | 168 | 246 | 468 |
| 15 | - | - | - | - | 56 | 75 | 109 | 284 | 61 | 82 | 118 | 298 | 102 | 136 | 199 | 406 |
| 16 | - | - | - | - | 46 | 62 | 89 | 248 | 50 | 67 | 96 | 261 | 84 | 112 | 163 | 356 |
| 17 | - | - | - | - | - | 52 | 73 | 219 | 42 | 56 | 80 | 230 | 70 | 93 | 135 | 315 |
| 18 | - | - | - | - | - | 43 | 61 | 195 | - | 47 | 66 | 205 | 59 | 79 | 112 | 280 |
| 20 | - | - | - | - | - | - | - | - | - | - | - | - | 43 | 57 | 80 | 225 |
| 22 | - | - | - | - | - | - | - | - | - | - | - | - | - | 43 | 59 | 185 |
| 24 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 26 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 28 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 30 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 32 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 34 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Span (ft) | $1^{3 / 4}{ }^{11} \times 11^{7 / 8^{\prime \prime}}$ |  |  |  | $1^{3 / 4}{ }^{11} \times 14^{\prime \prime}$ |  |  | Factored Total Resistance | $1^{3 / 4}{ }^{11} \times 16^{11}$ |  |  |  | $1^{3 / 4} 4^{\prime \prime} \times 18^{\prime \prime}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  |  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored <br> Total <br> Resistance |
|  | Live Load |  | $\begin{aligned} & \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \\ & \hline \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \end{aligned}$ |  |
|  | L/480 | L/360 |  |  | L/480 | L/360 |  |  | L/480 | L/360 |  |  | L/480 | L/360 |  |  |
| 6 | 1884 | - | - | 2386 | - | - | - | 3007 | - | - | - | 3674 | - | - | - | 4440 |
| 7 | 1186 | 1582 | - | 1944 | 1944 | - | - | 2419 | 2902 | - | - | 2917 | - | - | - | 3472 |
| 8 | 794 | 1059 | 1583 | 1598 | 1302 | 1736 | - | 2023 | 1944 | - | - | 2418 | 2768 | - | - | 2850 |
| 9 | 558 | 744 | 1110 | 1261 | 914 | 1219 | - | 1703 | 1365 | 1820 | - | 2064 | 1944 | - | - | 2417 |
| 10 | 407 | 542 | 808 | 1020 | 666 | 889 | 1326 | 1378 | 995 | 1327 | - | 1758 | 1417 | 1890 | - | 2097 |
| 11 | 305 | 407 | 605 | 842 | 501 | 668 | 995 | 1137 | 747 | 997 | - | 1451 | 1064 | 1419 | - | 1800 |
| 12 | 235 | 314 | 465 | 706 | 385 | 514 | 764 | 954 | 576 | 768 | 1144 | 1218 | 820 | 1093 | - | 1510 |
| 13 | 185 | 247 | 364 | 600 | 303 | 404 | 600 | 812 | 453 | 604 | 898 | 1036 | 645 | 860 | 1281 | 1285 |
| 14 | 148 | 197 | 290 | 517 | 243 | 324 | 479 | 698 | 362 | 483 | 717 | 892 | 516 | 688 | 1024 | 1106 |
| 15 | 120 | 160 | 235 | 449 | 197 | 263 | 388 | 607 | 294 | 393 | 581 | 776 | 420 | 560 | 830 | 962 |
| 16 | 99 | 132 | 192 | 394 | 162 | 217 | 318 | 533 | 243 | 324 | 478 | 680 | 346 | 461 | 683 | 844 |
| 17 | 82 | 110 | 159 | 348 | 135 | 181 | 264 | 471 | 202 | 270 | 397 | 602 | 288 | 384 | 568 | 747 |
| 18 | 69 | 93 | 133 | 309 | 114 | 152 | 221 | 419 | 170 | 227 | 333 | 535 | 243 | 324 | 477 | 665 |
| 20 | 50 | 67 | 95 | 249 | 83 | 111 | 159 | 338 | 124 | 165 | 240 | 432 | 177 | 236 | 345 | 536 |
| 22 | - | 50 | 70 | 204 | 62 | 83 | 118 | 277 | 93 | 124 | 178 | 355 | 133 | 177 | 257 | 441 |
| 24 | - | - | - | - | 48 | 64 | 89 | 232 | 72 | 96 | 136 | 297 | 102 | 136 | 196 | 369 |
| 26 | - | - | - | - | - | 50 | 68 | 196 | 56 | 75 | 105 | 251 | 80 | 107 | 152 | 312 |
| 28 | - | - | - | - | - | 40 | 53 | 168 | 45 | 60 | 82 | 215 | 64 | 86 | 120 | 268 |
| 30 | - | - | - | - | - | - | - | - | - | 49 | 65 | 186 | 52 | 70 | 95 | 232 |
| 32 | - | - | - | - | - | - | - | - | - | 40 | 52 | 162 | 43 | 57 | 77 | 202 |
| 34 | - | - | - | - | - | - | - | - | - | - | - | - | - | 48 | 63 | 178 |

## Notes:

1. The values in these tables meet the requirements of the National Building Code of Canada and CSA Standard 086-09 for dry service conditions and standard term loads. The live load must be greater than the dead load in order to use these tables.
2. All values listed are based on uniform loads applied to the top of the beam.
3. Span is defined as centre-to-centre of bearings and is valid for simple span and equal, continuous span conditions.
4. These tables assume full lateral support of the compression edge.
5. The designer must check both the Factored Total Resistance and the Total L/240 Deflection Resistance, AND the appropriate Live Load column, either the L/480 or L/360 deflection limit. Unfactored Deflection Resistance values that are blank are governed by the Factored Total Resistance.
6. The Unfactored Deflection Resistance for Total L/240 does not include the effects of long term loading (creep).
7. The total load values have been adjusted to account for the self-weight of the beam.
8. Proper bearing must be provided at each support. The required bearing can be determined from the Maximum Factored Reaction Table.
9. Depths of $16^{\prime \prime}$ or greater should be used with a minimum of two plies.
10. The values in this table are for a single ply of $13 / 4$ " LVL. Double the values for a 2 -ply ( $3^{1 / 2}{ }^{\prime \prime}$ thick) beam, triple the values for a 3 -ply ( $51 / 4$ " thick) beam, and quadruple the values for 4-ply (7" thick) beam.

## Uniform Load Resistance (plf) - 1.5E- Floor $100 \%-13 / 4$ " Width

| Span (ft) | $13 / 4{ }^{\prime \prime} \times 20^{\prime \prime}$ |  |  |  | $13 / 4^{\prime \prime} \times 22^{\prime \prime}$ |  |  |  | 13/4" $\times 24^{\prime \prime}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance |
|  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/240 } \end{aligned}$ |  | Live Load |  | $\begin{array}{l\|} \hline \text { Total } \\ \text { L/240 } \\ \hline \end{array}$ |  | Live Load |  | Total L/240 |  |
|  | L/480 | L/360 |  |  | L/480 | L/360 |  |  | L/480 | L/360 |  |  |
| 6 | - | - | - | 5329 | - | - | - | 6373 | - | - | - | 7616 |
| 7 | - | - | - | 4097 | - | - | - | 4803 | - | - | - | 5608 |
| 8 | - | - | - | 3326 | - | - | - | 3852 | - | - | - | 4436 |
| 9 | 2667 | - | - | 2799 | - | - | - | 3215 | - | - | - | 3669 |
| 10 | 1944 | - | - | 2415 | 2588 | - | - | 2758 | - | - | - | 3127 |
| 11 | 1460 | 1947 | - | 2124 | 1944 | - | - | 2414 | 2524 | - | - | 2724 |
| 12 | 1125 | 1500 | - | 1831 | 1497 | 1996 | - | 2146 | 1944 | - | - | 2413 |
| 13 | 885 | 1180 | - | 1558 | 1177 | 1570 | - | 1854 | 1529 | 2039 | - | 2165 |
| 14 | 708 | 944 | - | 1342 | 943 | 1257 | - | 1597 | 1224 | 1632 | - | 1872 |
| 15 | 576 | 768 | 1142 | 1167 | 766 | 1022 | - | 1389 | 995 | 1327 | - | 1629 |
| 16 | 474 | 632 | 939 | 1024 | 631 | 842 | - | 1219 | 820 | 1093 | - | 1430 |
| 17 | 395 | 527 | 781 | 906 | 526 | 702 | 1042 | 1078 | 683 | 911 | - | 1265 |
| 18 | 333 | 444 | 656 | 806 | 443 | 591 | 876 | 960 | 576 | 768 | - | 1126 |
| 20 | 243 | 324 | 476 | 651 | 323 | 431 | 636 | 775 | 420 | 560 | 827 | 909 |
| 22 | 182 | 243 | 355 | 536 | 243 | 324 | 475 | 638 | 315 | 420 | 619 | 749 |
| 24 | 140 | 187 | 271 | 448 | 187 | 249 | 363 | 534 | 243 | 324 | 474 | 627 |
| 26 | 110 | 147 | 211 | 380 | 147 | 196 | 283 | 453 | 191 | 254 | 370 | 532 |
| 28 | 88 | 118 | 167 | 326 | 117 | 157 | 224 | 389 | 153 | 204 | 294 | 456 |
| 30 | 72 | 96 | 134 | 282 | 95 | 127 | 180 | 337 | 124 | 165 | 236 | 396 |
| 32 | 59 | 79 | 108 | 246 | 78 | 105 | 146 | 294 | 102 | 136 | 193 | 346 |
| 34 | 49 | 65 | 88 | 217 | 65 | 87 | 120 | 259 | 85 | 113 | 158 | 305 |

Notes:

1. The values in these tables meet the requirements of the National Building Code of Canada and CSA Standard 086-09 for dry service conditions and standard term loads. The live load must be greater than the dead load in order to use these tables.
2. All values listed are based on uniform loads applied to the top of the beam.
3. Span is defined as centre-to-centre of bearings and is valid for simple span and equal, continuous span conditions.
4. These tables assume full lateral support of the compression edge.
5. The designer must check both the Factored Total Resistance and the Total L/240 Deflection Resistance, AND the appropriate Live Load column, either the L/480 or L/360 deflection limit. Unfactored Deflection Resistance values that are blank are governed by the Factored Total Resistance.
6. The Unfactored Deflection Resistance for Total L/240 does not include the effects of long term loading (creep).
7. The total load values have been adjusted to account for the self-weight of the beam.
8. Proper bearing must be provided at each support. The required bearing can be determined from the Maximum Factored Reaction Table.
9. Depths of $16^{\prime \prime}$ or greater should be used with a minimum of two plies.
10. The values in this table are for a single ply of $13 / 4$ " LVL. Double the values for a 2 -ply ( $31 / 2^{\prime \prime}$ thick) beam, triple the values for a 3 -ply ( $5 \frac{1}{4}$ " thick) beam, and quadruple the values for 4-ply (7" thick) beam.

### 1.5E LVL Uniform Load

Resistance (plf) - Roof $100 \% 1^{3 / 4} 4^{\prime \prime}$

## Uniform Load Resistance (plif) - 1.5 E- Roof $100 \%-13 / /^{"}$ Width

| Span <br> (ft) | $1^{3 / 4^{\prime \prime}} \times 7{ }^{1 / 4}{ }^{\prime \prime}$ |  |  |  | $1{ }^{3 / 4}{ }^{10} \times 91 / 4{ }^{1 /}$ |  |  |  | $1^{3 / 4^{\prime \prime}} \times 9^{1 / 2^{\prime \prime}}$ |  |  |  | $1^{3 / 4^{11}} \times 11^{1 / 4^{\prime \prime}}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  |  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | $\begin{array}{\|c\|} \hline \text { Factored } \\ \text { Total } \\ \text { Resistance } \end{array}$ |
|  | Live Load |  | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \\ & \hline \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | Total <br> L/180 |  |
|  | L/360 | L/240 |  |  | L/360 | L/240 |  |  | L/360 | L/240 |  |  | L/360 | L/240 |  |  |
| 6 | 571 | 857 | 1139 | 1158 | 1187 | - | - | 1722 | 1286 | - | - | 1781 | 2136 | - | - | 2218 |
| 7 | 360 | 540 | 716 | 850 | 747 | 1121 | - | 1325 | 810 | 1215 | - | 1391 | 1345 | - | - | 1814 |
| 8 | 241 | 361 | 478 | 649 | 500 | 751 | 997 | 1013 | 542 | 814 | - | 1064 | 901 | 1351 | - | 1448 |
| 9 | 169 | 254 | 335 | 512 | 351 | 527 | 698 | 799 | 381 | 571 | 757 | 839 | 632 | 949 | - | 1143 |
| 10 | 123 | 185 | 243 | 414 | 256 | 384 | 508 | 646 | 277 | 416 | 550 | 678 | 461 | 692 | 917 | 924 |
| 11 | 92 | 139 | 181 | 341 | 192 | 289 | 380 | 533 | 208 | 313 | 412 | 560 | 346 | 520 | 687 | 762 |
| 12 | 71 | 107 | 139 | 286 | 148 | 222 | 292 | 447 | 160 | 241 | 316 | 469 | 267 | 400 | 528 | 639 |
| 13 | 56 | 84 | 108 | 243 | 116 | 175 | 228 | 380 | 126 | 189 | 248 | 399 | 210 | 315 | 414 | 544 |
| 14 | 45 | 67 | 86 | 209 | 93 | 140 | 182 | 327 | 101 | 151 | 197 | 343 | 168 | 252 | 330 | 468 |
| 15 | - | 54 | 69 | 181 | 75 | 113 | 147 | 284 | 82 | 123 | 159 | 298 | 136 | 205 | 267 | 406 |
| 16 | - | 45 | 56 | 158 | 62 | 93 | 120 | 248 | 67 | 101 | 130 | 261 | 112 | 168 | 219 | 356 |
| 17 | - | - | - | - | 52 | 78 | 99 | 219 | 56 | 84 | 108 | 230 | 93 | 140 | 182 | 315 |
| 18 | - | - | - | - | 43 | 65 | 83 | 195 | 47 | 71 | 90 | 205 | 79 | 118 | 152 | 280 |
| 20 | - | - | - | - | - | 48 | 59 | 157 | - | 52 | 64 | 165 | 57 | 86 | 109 | 225 |
| 22 | - | - | - | - | - | - | - | - | - | - | - | - | 43 | 65 | 80 | 185 |
| 24 | - | - | - | - | - | - | - | - | - | - | - | - | - | 50 | 61 | 154 |
| 26 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 28 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 30 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 32 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 34 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| Span <br> (ft) | $1^{3 / 4}{ }^{11} \times 11^{7 / 8^{\prime \prime}}$ |  |  |  | $1^{3 / 4} 4^{\prime \prime} \times 14^{\prime \prime}$ |  |  |  | 13/4" $\times 16^{\prime \prime}$ |  |  |  | $1^{3 / 4} 4^{\prime \prime} \times 18^{\prime \prime}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance |
|  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  |
|  | L/360 | L/240 |  |  | L/360 | L/240 |  |  | L/360 | L/240 |  |  | L/360 | L/240 |  |  |
| 6 | - | - | - | 2386 | - | - | - | 3007 | - | - | - | 3674 | - | - | - | 4440 |
| 7 | 1582 | - | - | 1944 | - | - | - | 2419 | - | - | - | 2917 | - | - | - | 3472 |
| 8 | 1059 | 1589 | - | 1598 | 1736 | - | - | 2023 | - | - | - | 2418 | - | - | - | 2850 |
| 9 | 744 | 1116 | - | 1261 | 1219 | - | - | 1703 | 1820 | - | - | 2064 | - | - | - | 2417 |
| 10 | 542 | 814 | - | 1020 | 889 | 1333 | - | 1378 | 1327 | - | - | 1758 | 1890 | - | - | 2097 |
| 11 | 407 | 611 | 809 | 842 | 668 | 1002 | - | 1137 | 997 | - | - | 1451 | 1419 | - | - | 1800 |
| 12 | 314 | 471 | 622 | 706 | 514 | 771 | - | 954 | 768 | 1152 | - | 1218 | 1093 | - | - | 1510 |
| 13 | 247 | 370 | 488 | 600 | 404 | 607 | 802 | 812 | 604 | 906 | - | 1036 | 860 | - | - | 1285 |
| 14 | 197 | 296 | 389 | 517 | 324 | 486 | 641 | 698 | 483 | 725 | - | 892 | 688 | 1033 | - | 1106 |
| 15 | 160 | 241 | 315 | 449 | 263 | 395 | 519 | 607 | 393 | 589 | - | 776 | 560 | 840 | - | 962 |
| 16 | 132 | 198 | 259 | 394 | 217 | 325 | 427 | 533 | 324 | 486 | 640 | 680 | 461 | 692 | - | 844 |
| 17 | 110 | 165 | 214 | 348 | 181 | 271 | 354 | 471 | 270 | 405 | 532 | 602 | 384 | 577 | - | 747 |
| 18 | 93 | 139 | 180 | 309 | 152 | 228 | 297 | 419 | 227 | 341 | 447 | 535 | 324 | 486 | 639 | 665 |
| 20 | 67 | 101 | 129 | 249 | 111 | 166 | 215 | 338 | 165 | 248 | 323 | 432 | 236 | 354 | 463 | 536 |
| 22 | 50 | 76 | 95 | 204 | 83 | 125 | 160 | 277 | 124 | 186 | 241 | 355 | 177 | 266 | 345 | 441 |
| 24 | - | 58 | 72 | 171 | 64 | 96 | 121 | 232 | 96 | 144 | 184 | 297 | 136 | 205 | 264 | 369 |
| 26 | - | 46 | 55 | 144 | 50 | 75 | 94 | 196 | 75 | 113 | 143 | 251 | 107 | 161 | 206 | 312 |
| 28 | - | - | - | - | 40 | 60 | 74 | 168 | 60 | 90 | 112 | 215 | 86 | 129 | 163 | 268 |
| 30 | - | - | - | - | - | 49 | 58 | 145 | 49 | 73 | 90 | 186 | 70 | 105 | 130 | 232 |
| 32 | - | - | - | - | - | 40 | 47 | 126 | 40 | 60 | 73 | 162 | 57 | 86 | 106 | 202 |
| 34 | - | - | - | - | - | - | - | - | - | 50 | 59 | 142 | 48 | 72 | 87 | 178 |

## Notes:

1. The values in these tables meet the requirements of the National Building Code of Canada and CSA Standard 086-09 for dry service conditions and standard term loads. The live load must be greater than the dead load in order to use these tables.
2. All values listed are based on uniform loads applied to the top of the beam.
3. Span is defined as centre-to-centre of bearings and is valid for simple span and equal, continuous span conditions.
4. These tables assume full lateral support of the compression edge.
5. The designer must check both the Factored Total Resistance and the Total L/180 Deflection Resistance, AND the appropriate Live Load column, either the L/360 or L/240 deflection limit. Unfactored Deflection Resistance values that are blank are governed by the Factored Total Resistance.
6. The Unfactored Deflection Resistance for Total L/180 does not include the effects of long term loading (creep).
7. The total load values have been adjusted to account for the self-weight of the beam.
8. Proper bearing must be provided at each support. The required bearing can be determined from the Maximum Factored Reaction Table.
9. Depths of $16^{\prime \prime}$ or greater should be used with a minimum of two plies.
10. The values in this table are for a single ply of $13 / 4$ LVL. Double the values for a 2 -ply ( $3^{1 / 2}$ " thick) beam, triple the values for a 3 -ply ( $51 / 4$ "thick) beam, and quadruple the values for 4 -ply ( 7 " thick) beam.

## Uniform Load Resistance (plf) - 1.5E-Roof $100 \%-13 / 4$ " Width

| Span <br> (ft) | $1^{3 / 4}{ }^{\prime \prime} \times 20^{\prime \prime}$ |  |  |  | 13/4" $\times 22$ " |  |  |  | 13/4" $\times 24^{\prime \prime}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance | Unfactored Defl. Resistance |  |  | Factored Total Resistance |
|  | Live Load |  | Total L/180 |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  | Live Load |  | $\begin{aligned} & \hline \text { Total } \\ & \text { L/180 } \end{aligned}$ |  |
|  | L/360 | L/240 |  |  | L/360 | L/240 |  |  | L/360 | L/240 |  |  |
| 6 | - | - | - | 5329 | - | - | - | 6373 | - | - | - | 7616 |
| 7 | - | - | - | 4097 | - | - | - | 4803 | - | - | - | 5608 |
| 8 | - | - | - | 3326 | - | - | - | 3852 | - | - | - | 4436 |
| 9 | - | - | - | 2799 | - | - | - | 3215 | - | - | - | 3669 |
| 10 | - | - | - | 2415 | - | - | - | 2758 | - | - | - | 3127 |
| 11 | 1947 | - | - | 2124 | - | - | - | 2414 | - | - | - | 2724 |
| 12 | 1500 | - | - | 1831 | 1996 | - | - | 2146 | - | - | - | 2413 |
| 13 | 1180 | - | - | 1558 | 1570 | - | - | 1854 | 2039 | - | - | 2165 |
| 14 | 944 | - | - | 1342 | 1257 | - | - | 1597 | 1632 | - | - | 1872 |
| 15 | 768 | 1152 | - | 1167 | 1022 | - | - | 1389 | 1327 | - | - | 1629 |
| 16 | 632 | 949 | - | 1024 | 842 | - | - | 1219 | 1093 | - | - | 1430 |
| 17 | 527 | 791 | - | 906 | 702 | 1053 | - | 1078 | 911 | - | - | 1265 |
| 18 | 444 | 666 | - | 806 | 591 | 887 | - | 960 | 768 | - | - | 1126 |
| 20 | 324 | 486 | 638 | 651 | 431 | 647 | - | 775 | 560 | 840 | - | 909 |
| 22 | 243 | 365 | 476 | 536 | 324 | 486 | 637 | 638 | 420 | 631 | - | 749 |
| 24 | 187 | 281 | 365 | 448 | 249 | 374 | 488 | 534 | 324 | 486 | - | 627 |
| 26 | 147 | 221 | 285 | 380 | 196 | 294 | 381 | 453 | 254 | 382 | 497 | 532 |
| 28 | 118 | 177 | 226 | 326 | 157 | 235 | 303 | 389 | 204 | 306 | 396 | 456 |
| 30 | 96 | 144 | 182 | 282 | 127 | 191 | 244 | 337 | 165 | 248 | 319 | 396 |
| 32 | 79 | 118 | 148 | 246 | 105 | 157 | 199 | 294 | 136 | 205 | 261 | 346 |
| 34 | 65 | 98 | 121 | 217 | 87 | 131 | 164 | 259 | 113 | 170 | 215 | 305 |

## Notes:

1. The values in these tables meet the requirements of the National Building Code of Canada and CSA Standard 086-09 for dry service conditions and standard term loads. The live load must be greater than the dead load in order to use these tables.
2. All values listed are based on uniform loads applied to the top of the beam.
3. Span is defined as centre-to-centre of bearings and is valid for simple span and equal, continuous span conditions.
4. These tables assume full lateral support of the compression edge.
5. The designer must check both the Factored Total Resistance and the Total L/180 Deflection Resistance, AND the appropriate Live Load column, either the L/360 or L/240 deflection limit. Unfactored Deflection Resistance values that are blank are governed by the Factored Total Resistance.
6. The Unfactored Deflection Resistance for Total L/180 does not include the effects of long term loading (creep).
7. The total load values have been adjusted to account for the self-weight of the beam.
8. Proper bearing must be provided at each support. The required bearing can be determined from the Maximum Factored Reaction Table.
9. Depths of 16 " or greater should be used with a minimum of two plies.
10. The values in this table are for a single ply of $1^{3} / 4^{\prime \prime}$ LVL. Double the values for a 2 -ply ( $3^{1} / 2^{\prime \prime}$ thick) beam, triple the values for a 3 -ply ( $5^{1} / 4^{\prime \prime}$ thick) beam, and quadruple the values for 4-ply (7" thick) beam.

### 2.0 E Factored Column Axial Loads (lbs)

## Steel or Column Bearing

| Column Length (ft) | $31 / 2^{\prime \prime} \times 31 / 2^{\prime \prime}$ | $3^{1 / 2}{ }^{\prime \prime} \times 5112^{\prime \prime}$ | 3½" $\times 7$ " |
| :---: | :---: | :---: | :---: |
| 6 | 18875 | 29661 | 37750 |
| 7 | 15732 | 24721 | 31463 |
| 8 | 13061 | 20525 | 26122 |
| 9 | 10843 | 17038 | 21685 |
| 10 | 9015 | 14167 | 18031 |
| 11 | 7513 | 11806 | 15026 |
| 12 | 6277 | 9864 | 12554 |
| 13 | 5261 | 8267 | 10521 |
| 14 | 4424 | 6953 | 8849 |
| > 14 | Not Permitted | Not Permitted | Not Permitted |



Column to beam connection
by design professional

Column base not shown; verify capacity with manufacturer

## Notes:

1. This table has been prepared in accordance with the National Building Code of Canada and CSA Standard 086-09 for standard term loads and dry service conditions.
2. The compressive resistance is based on the following assumptions:

- The effective column height is the clear height of the column between the top and bottom supports.
- Columns are braced in both directions at the top and bottom supports.
- The vertical load is applied with an eccentricity of $1 / 6$ of the column width or depth, whichever controls.
- No lateral loads are applied to the column.
- No notching or drilling except as required for the installation of the column caps or bases.

3. These tables are for solid one-piece members. Built-up columns are beyond the scope of the tables.
4. Steel bearing refers to end-grain bearing of the column on a steel plate or beam designed by others to adequately carry the column load.
5. SPF plate bearing refers to bearing of the column on $1 \frac{1}{2}$ " thick Spruce-Pine-Fir dimension lumber plate ( $\mathrm{fcp}=769 \mathrm{psi}$ ). For other conditions, the designer must check the compressive resistance of the bearing material. No increase is allowed with out a complete analysis of the column resistance.

## Connection Details

Beam-to-Beam Connection


Install hanger per manufacturer's instructions. Hanger must distribute load to each ply of the assemble. Contact International Beams, Inc. technical support with questions.

Beam Pocket in Masonry Wall


Protect LVL from moisture with a vapor barrier and airspace. LVL should not directly contact contact concrete.


Install column cap per manufacturer's instructions; verify cap and column capacity.

## Bearing on Exterior Wall



LVL should not directly contact concrete. Verify plate bearing capacity on page 19.

Bearing for Door or Window


Strap per building code if top plate is not continuous over header.

Solid Blocking at Post


Provide a continuous load path to concrete.

## Minimum Nail Spacing

for nails installed parallel to the glueline

| Nail Size | Single Row | Multiple Rows ${ }^{1}$ |
| :---: | :---: | :---: |
| 8d Common ( ¹⁄2 $^{\text {" }}$ ) | $3 "$ | $4 "$ |
| 10d Common (3") | $4 "$ | 5" |
| 12d Common ( $3^{1 / 4} 4^{\prime \prime}$ ) | $4 "$ | 5" |
| 16d Common ( $31 / 22^{\prime \prime}$ ) | $5 "$ | $6{ }^{\prime 2}$ |

1. Offset multiple rows $1 / 2^{\prime \prime}$ and stagger nails on equal-equal layout
2. Minimum nail spacing may be reduced to $5^{\prime \prime}$ for $13 / 4$ " wide members
3. Nail penetration shall not exceed $21 / 2^{\prime \prime}$ for 10 d and 12 d nor $2^{\prime \prime}$ for 16 d

## Multiple Piece Assembly \& Side Load Capacity

When assembling more than one LVL ply into a single load-bearing beam, follow the appropriate guidelines:


Max. Factored Uniform Load Applied to Either Outside Piece (plf)

| Connection Detail | 2 Rows of $3^{1 / 2 "}$ <br> Spiral Nails at 12" oc | 3 Rows of $3^{1 / 1 / 2 "}$ <br> Spiral Nails at $12{ }^{\prime \prime}$ oc | 2 Rows of $1 / 2^{\prime \prime}$ dia. Bolts at 24 " oc | 2 Rows of $1 / 2^{\prime \prime}$ dia. Bolts at 12 "oc |
| :---: | :---: | :---: | :---: | :---: |
| A | 788 | 1182 | 680 | 1360 |
| B | 591 | 887 | 510 | 1020 |
| C | - | - | 453 | 907 |
| D | Refer to Simpson Strong-Tie catalog for SDS capacities |  |  |  |
| E | - | - | 1362 | 2724 |

Notes:

1. The values have been calculated in accordance with CSA 086-09 for standard term loads and dry service conditions.
2. Use the sizing software or load tables to size the beam, then determine the required fastening.
3. The specified nailing applies to both faces of a 3 ply beam.
4. Four ply beams may not be loaded from one side only. They must be loaded from both sides or top loaded.
5. $3^{1} / 2^{\prime \prime}$ spiral nails shall have a diameter of $0.152^{\prime \prime}$
6. Bolts shall conform to ASTM A307. Bolt holes must be centered at least two inches from the top and bottom edges of the beam. Washers must be used under the bolt heads and nuts. Offset or stagger rows of bolt holes by one-half of the bolt spacing.
7. Use 3 rows of nails for beams between 12 "and 18 "deep.

Maximum Factored Reaction (Ibs)

| Bearing Length |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width (in) ${ }^{1}$ | 11/2" | 2" | 21/2" | 3" | 31/2" | 4" | 41/2" | 5" | 51/2" | $6 "$ | 61/2" | 7" | 71/2" | 8" | 81/2" | 9" | 91/2" | 10" | 101/2" | 11" | 111/2" | 12" |
| 13/4" | 2870 | 3820 | 4780 | 5730 | 6690 | 7640 | 8600 | 9560 | 10510 | 11470 | 12420 | 13380 | 14330 | 15290 | 16240 | 17200 | 18150 | 19110 | 20070 | 21020 | 21980 | 22930 |
| $3^{11 / 2 "}$ | 5730 | 7640 | 9560 | 11470 | 13380 | 15290 | 17200 | 19110 | 21020 | 22930 | 24840 | 26750 | 28670 | 30580 | 32490 | 34400 | 36310 | 38220 | 40130 | 42040 | 43950 | 45860 |
| 51/4" | 8600 | 11470 | 14330 | 17200 | 20070 | 22930 | 25800 | 28670 | 31530 | 34400 | 37260 | 40130 | 43000 | 45860 | 48730 | 51600 | 54460 | 57330 | 60200 | 63060 | 65930 | 68800 |
| 7" | 11470 | 15290 | 19110 | 22930 | 26750 | 30580 | 34400 | 38220 | 42040 | 45860 | 49690 | 53510 | 57330 | 61150 | 64970 | 68800 | 72620 | 76440 | 80260 | 84080 | 87910 | 91730 |

## Notes:

1. Use any combination of $13 / 4^{\prime \prime}$ and $3^{1} / 2^{\prime \prime}$ members using proper nailing or bolting guidelines.
2. Minimum bearing length is $11 / 2^{\prime \prime}$. Bearing across the full width of the beam is required.
3. The tabulated values are based on the compressive perpendicular to grain strength of the LVL. ( $\mathrm{F}_{\mathrm{cp}}=1365 \mathrm{psi}$ ), Beams bearing on \#2 and better, 2 x plates must be increased by the following factor:

| Spruce-Pine-Fir | 1.78 |
| :--- | :--- |
| Douglas Fir-L | 1.35 |
| Hem-Fir | 2.05 |

4. Values are in accordance with CSA 086-09 for standard term loads and dry service conditions.

## Handling and Storage Guidelines

- LVL should be protected from the weather and stored lying flat.
- Product must not be stored in contact with the ground.
- Store LVL in wrapped bundles, provide air circulation and support bundles with $2 x 4$ stickers.
- Protect from the weather on the job site both before and after installation. LVL is intended for use in covered, dry conditions only.
- Except as described in this product guide, LVL should not be cut, drilled or notched.
- Do not install wet or visually damaged product.



## Sizing Software

To better assist engineers, designers and specifiers, International Beams, Inc. has partnered with Keymark of Boulder Colorado, an industry leader in design software to provide KeyBeam® ${ }^{\circledR}$. This single member sizing system will aid in the specification of framing members to structurally resist engineering problems described by the software user.

KeyBeam recognizes the National Building Code of Canada (NBCC) and offers printable design calculations and beam capabilities. The software user can specify simple span applications, point loads, cantilevers and many more common applications. Please contact International Beams, Inc. Sales to learn more about receiving a complimentary copy of KeyBeam Software.

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