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Services

China Nuclear Power Engineering Co.,Ltd.

# Beyond Design Code, Introduction of Defect Tolerance Assessment of UK HPR1000

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Natural Energy Powering Nature

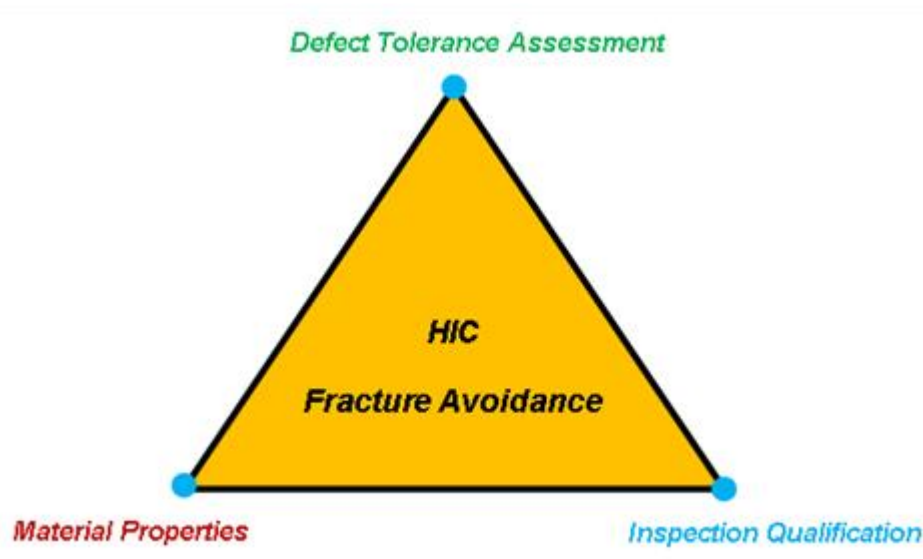
## **Comprehensive of terminology “structural integrity” in UK:**

- a) A much more wider range than China practice whereas mainly mechanical analysis is focused in China practice.
- b) No design codes & standards specified, and codes & standards are not enough.
- c) Demonstrated by “safety case”.

**Besides design codes & standards, the UK HPR1000 also considers UK context. In terms of stress and assessment, it is mainly called ‘Avoidance of Fracture’.**

**The avoidance of fracture demonstrates that the High Integrity Components are tolerant of defects to through-life degradation**

The integration of DTA, high reliability NDT and lower bound material properties support the avoidance of fracture demonstration



❑ **Defect tolerance assessment / DTA**

$$DSM = ELLDS / (QEDES + LFCG) \geq 2$$

<i>DSM:</i>	<i>Defect Size Margin</i>
<i>ELLDS:</i>	<i>End of Life Limiting Defect Size</i>
<i>QEDES:</i>	<i>Qualified Examination Defect Size</i>
<i>LFCG:</i>	<i>Life time Fatigue Crack Growth</i>

❑ ***DTA main Procedure is following:***

- 1. Material property determination*
- 2. Classify loadings and consequences stresses*
- 3. Defect characterization*
- 4. Analysis type selection (crack initiation or tearing )*
- 5. Determine final defect size (crack fatigue crack growth)*
- 6. Determine end of life limiting defect size*
- 7. DSM target check and refinement*

❑ **Characteristic of DTA:**

1. FAD diagram method, no safety factor inherent (R6 procedure)
2. Conservative material properties assumption
3. Conservative loads and loads combination
4. Residual stresses involved

## □ **Loading**

1. Steady load, dead weight, mechanical loads and thermal loads
2. Transients load, pressure, thermal and flow rate transients
3. Residual stresses
4. others

## □ **Stress and SIF**

The stresses arising from loadings should be divided into primary stresses and secondary stresses according to the contribution to plastic collapse. Due to the interaction between primary and secondary stresses, a coefficient will be applied to Stress Intensity Factor (SIF) caused by secondary stresses, and then combined with SIF resulted by primary stresses.

## ❑ **Defect Characterisation**

For defect tolerance assessment in GDA, only surface planar flaws are assumed.  
The flaw depth, width and shapes cause different stress intensity factor forms.

## ❑ **Analysis Type Selection**

### ✓ Crack initiation

Base analysis type for all conditions.

### ✓ Crack tearing

Alternative analysis type for emergency and fault condition.



□ **Determine Final Defect Size**

✓ Fatigue Crack Propagation

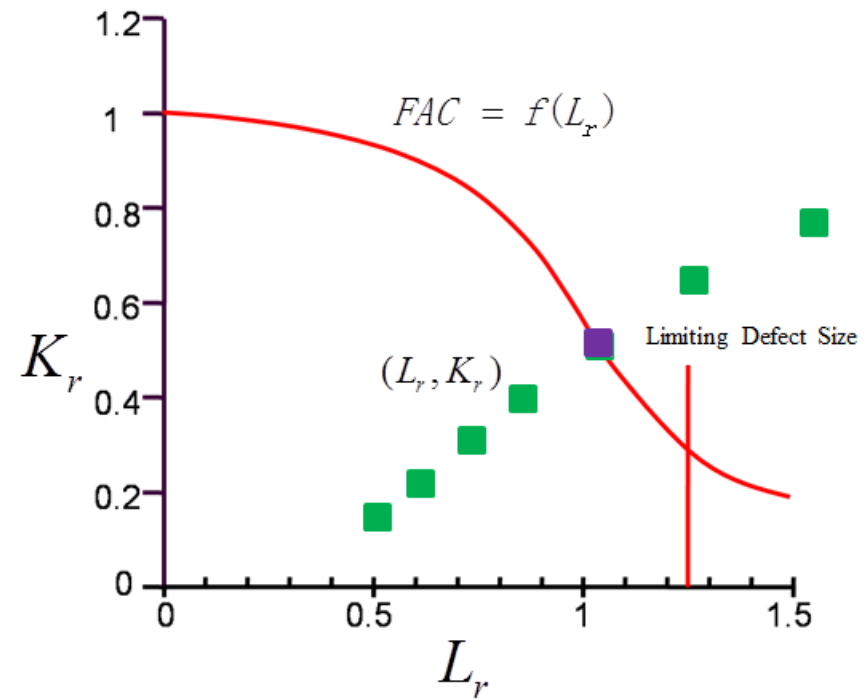
Paris Law is introduced for fatigue crack growth.

$$da / dN = A(\Delta K)^m$$

Final defect size = initial crack size + fatigue crack growth

□ **Determine ELLDS**

If the point  $(L_r, K_r)$  is on FAC, or a little bit below, the responding defect size can be defined as limiting defect size.



## □ **FAC Curves Selection**

1. R6 offers three types of failure assessment curves, named option 1, 2 and 3.
2. For conservative purpose, it is prior to select option 1 for DTA. If option 1 is too conservative, option 2 and 3 are the candidate options.
3.  $Lr(\max)$  could be determined as following approximately:

$$Lr(\max) = (\sigma_y + \sigma_u) / 2\sigma_y$$

## □ *L<sub>r</sub> and K<sub>r</sub>*

L<sub>r</sub> is defined as following

$$L_r = \frac{P}{P_L} = \frac{\sigma_{ref}}{\sigma_y}$$

Involved a coefficient V, the combination of primary and secondary SIF are defined as following:

$$K_r = \frac{K_I^P}{K_{mat}} + \frac{VK_S^P}{K_{mat}}$$

□ DSM Check

1. Amount of crack tearing instead of initiation in Level D
2. More realistic material property in some cases
3. Selection of more realistic FAC curve while in large  $L_r$  regime
4. Alternative methods

*Thanks*